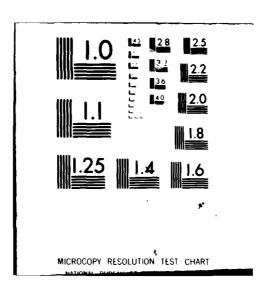
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# **DAVID W. TAYLOR NAVAL SHIP** RESEARCH AND DEVELOPMENT CENTER Bethesda, Md. 20084 MODIFICATIONS TO COMPUTER



MODIFICATIONS TO COMPUTER PROGRAM FOR PARAMETER ESTIMATION FOR THE GENERALIZED GAMMA DISTRIBUTION

by

Michel K. Ochi

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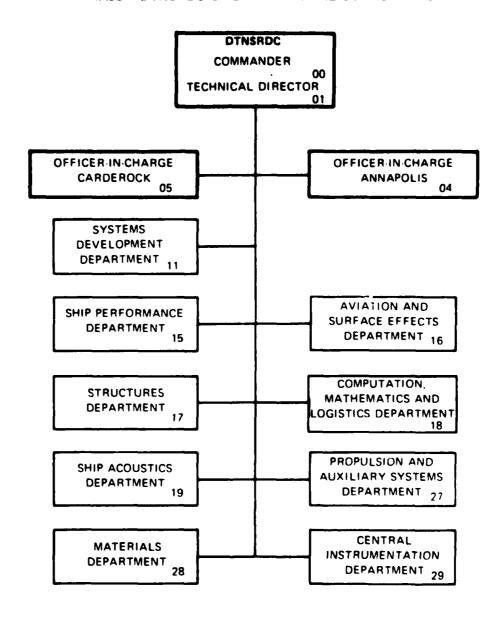
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May 1977

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MODIFICATIONS TO COMPUTER PROGRAM FOR PARAMETER ESTIMA' FOR THE GENERALIZED GAMMA DISTRIBUTION

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An extensive study of an existing digital computer program for determining parameters required to represent SES 100B trials data by a generalized gamma function is carried out. The purpose of the study is to resolve the difficulties encountered in earlier studies. In these earlier studies, approximately 5 percent of the cases analyzed produced unrealistic values for the distribution parameters. In order to resolve this problem, data sensitivity studies are carried out. Based on results of the study, criteria are developed for determining cases that should not be processed. Three other techniques besides

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# TABLE OF CONTENTS

	•				Page
ABSTRACT		•		•	1
ADMINISTRATIVE INFORMATION					1
INTRODUCTION		•			1
MATHEMATICAL DEVELOPMENT	•				4
OVERVIEW		•	•	•	4
MAXIMUM LIKELIHOOD METHOD				•	5
ANALYSIS					8
SENSITIVITY OF RESULTS ON EXPERIMENTAL DATA	١.			•	10
EVALUATION OF MAXIMUM LIKELIHOOD METHOD		•		•	13
DIGITAL PROGRAM DESCRIPTION		•	•		14
INPUT DATA			•		16
PRINTED OUTPUT			•	•	22
PROGRAM DESCRIPTIONS			•	•	24
Main Program	•	•	•		24
Subroutine GETCML	•	•	•		27
Subroutine MLHCML	•	•		•	30
Subroutine DIST	•	•			32
Subroutine WEG	•	•	•	•	33
Function PSI1	•	•	•	•	34
Function PSI2	•	•	•		35
Function PSI		•	•	•	36
Subroutine MGAMMA	•	•	•	•	37
Subroutine MDGAM					38

	Page
Subroutine HISTO	38
Function G	39
Function F	40
CONCLUSIONS	41
ACKNOWLEDGEMENTS	42
REFERENCES	43
APPENDIX A - PROGRAM LISTING	A-1
APPENDIX R - EXAMPLE OF PRINTOUT	R_1

# LIST OF ILLUSTRATIONS

		Page
FIGURE		
1	A COMPARISON OF THE GENERALIZED GAMMA DISTRIBUTION WITH EXPERIMENTAL DATA	9
2	A COMPARISON OF THE GENERALIZED GAMMA DISTRIBUTION AS DETERMINED BY THE MAXIMUM LIKELIHOOD METHOD WITH EXPERIMENTAL DATA	15
3	CARD IMAGES FOR A TYPICAL COMPUTER RUN	21
TABLE		
1	RESULTS OF SENSITIVITY STUDY ON FOUR REPRESENTATIVE CASES	12
2	MAJOR FORTRAN SYMBOLS USED IN MAIN PROGRAM	25
3	MAJOR FORTRAN SYMBOLS	28

### ABSTRACT

An extensive study of an existing digital computer program for determining parameters required to represent SES 100B trials data by a generalized gamma function is carried out. The purpose of the study is to resolve the difficulties encountered in earlier studies. In these earlier studies, approximately 5 percent of the cases analyzed produced unrealistic values for the distribution parameters. In order to resolve this problem, data sensitivity studies are carried out. Based on results of the study, criteria are developed for determining cases that should not be processed. Three other techniques besides the Stacy-Mihram method are investigated. The most successful alternative method is the maximum likelihood method, which is incorporated into the new digital computer program. A program listing and an example of the generated output are included in this report.

#### ADMINISTRATIVE INFORMATION

This work was conducted at the David W. Taylor Naval Ship Research and Development Center and authorized by Naval Sea Systems Command, Surface Effect Ships Project Office, Program Element Number 63534N. It is identified as Work Unit Number 1-1506-012.

#### INTRODUCTION

A computerized procedure for evaluating the parameters of the generalized gamma distribution from a set of random data following the method proposed by Stacy and Mihram (see Reference 1) has been previously

developed and extensively exercised (see Reference 2 and 3). During these earlier studies it was discovered that what appeared to be unrealistic values for the distribution parameters were obtained in roughly 5 percent of the cases analyzed. The initial purpose of the study, whose results are summarized in this report, was to explore in detail a representative sample of cases resulting in unrealistic values of the parameters, and if possible, to develop an alternate method for processing these cases.

The results of the present investigation can be summarized as follows:

- a. In the many cases studied, it appears that the predicted extreme design values are most sensitive to experimental measurements and not the numerical procedure for determining the parameters. This is particularly true when one of the parameters is negative.
- b. All four methods considered in this investigation yield probability distribution functions which represent very well the experimentally obtained histogram even though some of the parameter values were judged unrealisitic in previous studies. However, the Stacy-Mihram and maximum likelihood methods are by far the most efficient and are the preferred procedures based on probabilistic arguments.
- c. In some cases the predicted extreme design values are unrealistically large whereas the significant values are

realistic. Based on an analysis of over 100 cases, it can be concluded that cases having a nondimensional third logarithmic moment greater than -0.5 produce unrealistic extreme design values. Results of a data sensitivity study have revealed that in all these cases the data may not be considered as a sample taken from a steady-state random phenomenon, and hence it is recommended not to carry out statistical analysis for these cases.

# MATHEMATICAL FORMULATION

## **OVERVIEW**

The generalized gamma density function under consideration in this report has the form

$$f(x; \lambda, m, c) = \frac{c \lambda^{cm}}{\Gamma(m)} x^{cm-1} e^{(-(\lambda x)^c)}$$
 (1)

where  $\lambda$ , m, and c are estimation parameters and  $\Gamma(m)$  is the gamma function. Many other distributions such as the exponential, gamma, chi-squared, Weibul, hydrograph, chi, truncated normal, and Rayleigh are special cases of the generalized gamma function. Due to the general nature of  $f(x; \lambda, m, c)$ , it is the preferred distribution particularly when the exact form of the distribution function is unknown.

There are several techniques that can be used to estimate the three parameters. Four such techniques are considered in this effort. These are the Stacy-Mihram, the maximum likelihood, the nonlinear least squares, and grid search methods. The last two methods determine the parameters by searching for that set of parameters resulting in a minimum error between the experimental and theoretical histograms. Since statistical inference cannot be applied in a rigorous manner, the last two methods are not recommended. The Stacy-Mihram method determines the parameters by requiring that the first three theoretical logarithmic moments agree with the logarithmic moments determined from the experimental data. The maximum likelihood method determines parameters such that the joint probability density function is a maximum.

A detailed derivation of the Stacy-Mihram method is presented in Reference 2 pages 6-8. A derivation of the nonlinear least squares procedure is presented in Reference 4. The grid search procedure merely involves a systematic search of the  $\lambda$ , m, c space for parameters that minimize the error between the predicted distribution and the measured distribution. A derivation of the equations required in the maximum likelihood parametric estimation method is presented in the next section. MAXIMUM LIKELIHOOD METHOD

Briefly, the maximum likelihood estimation technique involves finding the parameter (or parameters) which maximizes the joint probability density function of a random sample  $X_1, \ldots, X_N$  from a distribution with  $f(x, \theta)$  as its probability density function and  $\theta$  as an element of the parameter space. The joint probability density function, referred to as the likelihood function, is given by

$$L = \prod_{i=1}^{n} f(\chi_{i}; \theta)$$
 (2)

Assume one has N samples at random variable  $\mathbf{x}_i$ . Then the maximum likelihood function will have the form

$$L = \prod_{i} f(x_{i}, \theta)^{n_{i}}$$
 (3)

The natural logarithm of the likelihood function is used in maximizing since it is a maximum when the function itself is a maximum, and it proves more convenient to use. The logarithm is given by,

$$\ln L = \sum_{i=1}^{K} N_i \ln f(x_i)$$
 (4)

The maximum of lnL is obtained by searching for parameters  $\theta$  such that,

$$\frac{\partial \ln L}{\partial \theta_i} \bigg|_{i=1,N_0} = 0.0 \tag{5}$$

where  $N_p$  = the number of parameters.

For the generalized gamma function given by Equation (1), the likelihood function becomes

$$L = \prod_{i=1}^{K} \left[ \frac{c \lambda_{c_{i}} x_{i_{c_{i}}}}{\Gamma(m)} e^{(-(\lambda_{i} x_{i})^{c})} \right]^{N_{i}}$$
 (6)

and InL becomes

$$\ln L = N \ln c + cm N \ln \gamma - N \ln \Gamma(m)$$

$$+ (cm-1) \leq N_1 \ln \chi_1 - \gamma^2 \leq \chi_1^2 N_1$$
(7)

In the above equation, c is assumed positive. If the above equation is differentiated with respect to cm,  $\lambda$  and m and set to zero, the following equations can be derived (see Reference 5).

$$\ln c + \ln \left( \sum_{i} x_{i}^{c} N_{i} \right) - \ln c m - \ln N + \psi(m)$$

$$- c \sum_{i} N_{i} \ln x_{i} / N = 0$$
(9)

$$/m + \Psi(m) - lncm + lnc + ln( \leq x_i \in N_i)$$
  
-  $ln N - c \leq (ln x_i (x_i N_i)) / \leq x_i \in N_i = 0$  (10)

where the summation on i is from 1 to K. An expression for m can be obtained from the above equations:

$$\sqrt{W} = C \left[ \frac{\sum x'_{\epsilon} N'_{\epsilon}}{\sum (J_{\nu} x'_{\epsilon})(X'_{\epsilon} N'_{\epsilon})} - \frac{N}{\sum N'_{\epsilon} J_{\nu} x'_{\epsilon}} \right]$$
(11)

The parameter c can be obtained by solving the following equation numerically.

$$\ln c + \ln \left( \sum_{i} x_{i}^{c} N_{i} \right) + \ln \left[ \frac{\sum_{i} (\ln x_{i}^{c}) \left( x_{i}^{c} N_{i}^{c} \right)}{\sum_{i} x_{i}^{c} N_{i}} - \frac{\sum_{i} N_{i} \ln x_{i}^{c}}{N} \right]$$
(12)

$$-\ln N + \Psi\left[\frac{1}{C\left(\frac{\epsilon(\ln x_i)(x_i^*N_i)}{N} - \frac{\epsilon N_i \ln x_i}{N}\right)}\right] - \frac{c \epsilon N_i \ln x_i}{N} = 0$$

Once a value of c is determined by solving Equation (12), values for  $\lambda$  and m can be obtained via Equations (8) and (11). The numerical method used to solve Equation (12) for c is due to Wegstein (see Reference 5).

#### **ANALYSIS**

During previous studies in which the Stacy-Mihram method was used to process SES 100B data, large design extreme values were predicted in approximately 5 percent of the cases although the most significant values agreed with the experimental measurements. This difficulty seemed to be associated with large values of the parameter m and with negative values of the parameter c. In order to resolve this difficulty, several cases were examined in detail. The results of this investigation follows.

The first case considered in this investigation is a set of pitching motion data measured during the SES 100B full scale trials program at 30 kts in a seastate of 3. This particular case, identified as AR1 3E 30, is presented in Reference 3. A comparison of the estimated probability density function with the experimental histogram is presented in Figure 1. As is demonstrated by the results in the figure, the agreement is excellent. All other cases examined show similar results. Assuming that an objective of the estimation procedure is to develop the best representation of the data that is possible, it is concluded that large values of m(> 5) are not necessarily unreasonable.

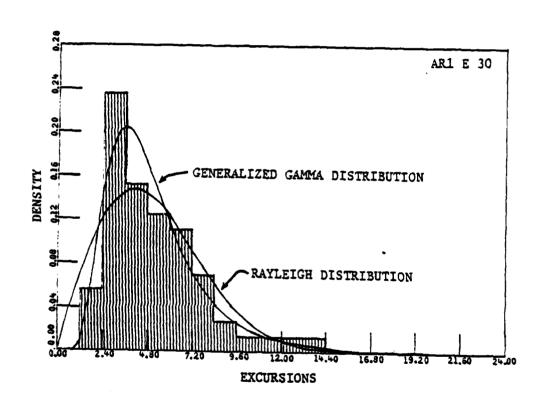


FIGURE 1. A COMPARISON OF THE GENERALIZED GAMMA DISTRIBUTION WITH EXPERIMENTAL DATA

Also, since the predicted representations always represent the data very well for both large and small m, the numerical procedure used to solve the transcendental equations for the estimation parameters is judged sufficiently accurate.

Further investigations revealed that in some of the cases the predicted design extreme values were unreasonably high as compared with the most significant values. In order to determine more precisely a reasonable value for the ratio of the design extreme value to the most significant value  $(X_D/X_S)$ , an analysis of over 100 previously processed data cases were examined. The results indicated that unrealistically large ratios were obtained for those cases for which the normalized logarithmic moment (see Equation 2.4 in Reference 2) is greater than -0.5. Most significant values were realisitic as compared with those measured in trials. Consequently, in the current data base, cases for which T > -0.5 should not be processed to determine design extreme values using the generalized gamma procedure.

The experimental histogram of AR1 3E 30 has a substantial tail which may contribute to the large design extreme value prediction. The last four bins (out of 12) each have only one observation. A data sensitivity study was conducted in order to determine how sensitive the design values are to the tail portion of the measured data. The results of this study are presented in the next section. SENSITIVITY OF RESULTS ON EXPERIMENTAL DATA

A data sensitivity study on cases AR1 3E 30, S14 3H 10, S14 3Q 10, and S82 3Q 10 was carried out in order to make an assess-

ment of how sensitive predicted results are to the experimental data. Computations were carried out for several cases for which four observations from a rather distinct tail were dropped. The results are presented in Table 1.

The results indicate that elimination of a small percentage of the experimental data can result in large changes in the design extreme value, particularly when T > -0.5 and c < 0.0. Based on these results, it appears that a substantially large number of observations in the tail portion of the experimental data is desirable in order to predict results that are insensitive to minor errors in the observations.

It should be noted that the data sensitivity study as conducted above is rather severe, i.e., four points were removed in a systematic manner from the tail portion of the measured histogram. The probability that four points from the tail would be incorrectly measured is rather small. One way of determining how long an experiment should be conducted and consequently how many observations should be made is to monitor various statistics such as moments during any particular experiment. Once these statistical measures reach steady state, the sample can be judged adequate. Proceeding in this manner may have been impractical during a single prototype run. However, combining several runs under nearly identical experimental conditions may prove possible.

TABLE 1

RESULTS OF SENSITIVITY STUDY ON FOUR REPRESENTATIVE CASES

%∆X <sub>S</sub>	-15%	-8%	-17%	-28%
%∆X <sub>D</sub>	-42	-21	-93	-59
z	99 20	209 205	131	63 59
x <sub>D</sub> /x <sub>s</sub>	3.56	6.93 5.95	19.0 11.9	17.1
o <sub>x</sub>	29.16 16.80	174.0 137.8	155.0 80.4	85.3 35.2
×°	8.19 6.96	25.12 23.15	8.18 6.77	5.0 3.6
~	$0.2 \times 10^{-10}$ $123.3$	209.0 13.9	$0.1 \times 10^{-2}$ $0.5 \times 10^{-6}$	$0.3 \times 10^{-3}$ 0.6 × 10 <sup>-9</sup>
U	-0.21 0.50	0.33	-0.37	-0.31
E	105. 23.	11.9	9.7	11.8
CASE	AR1 3E 30	S14 3H 10	S14 3Q 10	582 30 10

## EVALUATION OF THE MAXIMUM LIKELIHOOD METHOD

The method previously employed to determine estimation parameters for the generalized gamma distribution was based on the Stacy-Mihram method (see Reference 1 and 2). One of the advantages of the Stacy-Mihram method is that negative values of the parameter c are allowed. However, based on the current analysis of over 100 cases, it appears that cases for which c is negative result in unrealistically large values of the ratio of the design extreme value to the significant value regardless of the processing technique (Stacy-Mihram method, grid search, nonlinear least squares method). Consequently, development of representations of the experimental via the generalized gamma function should be restricted to cases for which the parameter c > 0. More detailed analysis (see comments at the beginning of this section) has revealed that processing should be restricted to those cases for which the normalized logarithmic moment is less than -0.5\*. If the above restrictions are imposed, the preferred processing method is the maximum likelihood method as developed in a previous section of this report. One of the reasons the maximum likelihood method is preferred is that it provides unbiased and efficient parameter estimates in the asymptotic limit, i.e., as the number of samples becomes

<sup>\*</sup>Examination of the data shows that it cannot be adequately represented by any of the standard distributions.

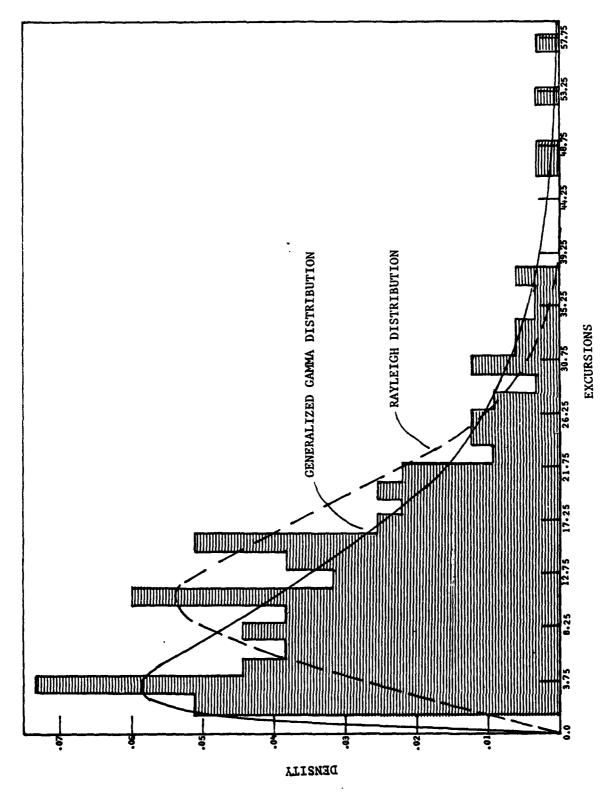
large, provided specified regularity conditions hold (see References 6 and 7 for details). Also, the method is applied to the actual experimental measurements, i.e., grouping the data into histograms is not necessary.

A comparison of the maximum likelihood results with experimental data is presented in Figure 2. As demonstrated by the figure, the agreement between the generalized gamma representation and the experimental data is excellent. The ratio of design extreme value to most significant value is 3.65 which is less than the value obtained by the Stacy-Mihram method is 5.58.

#### DIGITAL PROGRAM DESCRIPTION

The current digital program is based on a previous program that implemented the Stacy and Mihram method. The following modifications have been made:

1. The maximum likelihood method has been incorporated into the previous program. This is accomplished by replacing subroutine GETCML with a new version. The maximum likelihood method should be used only when the numbers of observations is greater than 100, or the number of bins is greater than 60. The Stacy-Mihram method should be used when the number of bins is less than 20 and the number of observations is greater than 100.



A COMPARISON OF THE GENERALIZED GAMMA DISTRIBUTION AS DETERMINED BY THE MAXIMUM LIKELIHOOD METHOD WITH EXPERIMENTAL DATA 5. FIGURE

- As an added option, data can be read in the form of densities or counts per bin.
- Printer plots of Rayleigh, generalized gamma function, and experimental data are generated.
- 4. Since the extreme values are a function of the number of observations (time), time effect plots are generated along with tabular results.

Three proprietary programs supplied by DTNSRDC are used in the present system. These are PLOTPR, MGAMMA, and MDGAM. PLOTPR is used to produce printer plots of data written on unit 3, MGAMMA computes the gamma function, and MDGAM computes the incomplete gamma function. Printer plot programs and programs for the gamma function are readily available on most computer systems. Hence, replacing these with programs available at different installations should present no major difficulties. The incomplete gamma function can be obtained from the gamma function via a simple integration procedure. However, due care must be exercised to assure sufficient numerical accuracy.

A complete description of input data, printed output, and subroutines follows. A listing of the program is presented in Appendix A. An example of print out is presented in Appendix B.

INPUT DATA

A description of input data follows. Card images of a typical run stream are illustrated in Figure 3.

Card	<u>Variable</u>	Cols.	Format	Description
1	IC(1)	1-2	12	option to convert input data from frequencies to densities.  H <sub>NEW</sub> = H <sub>OLD</sub> /(N x DEL)  ON: IC(1) = 1
2	IC(2)	3-4	12	option to convert L values from time to sample/run time L <sub>NEW</sub> = (L <sub>OLD</sub> /Run time) x N ON: IC(2) = 1
3	IC(3)	5-6	12	option to change random variable values ON: IC(3) = 1
1	IC(4)	7-8	12	option to convert input data by factor CAL ON: IC(4) = 1
1	IC(5)	9-10	12	option to plot Histogram, Rayleigh and Gamma with "PLOTPR" ON: IC(5) = 1
1	IC(6)	11-12	12	option to plot above in MKS units (change by factor CONVER) ON: IC(6) = 1
1	IC(7)	13-14	12	option to plot L in hours vs. X <sub>D</sub> , X <sub>G</sub> (Time effect plots)
				ON: IC(7) = 1
1	IC(8)	15-16	12	option to plot above in MKS units ON: IC(8) = 1
1	IC(9)	17-18	12	option to print gamma functions for all L values OFF: IC(9) = 1 ON: otherwise

Card	<u>Variable</u>	Cols.	Format	Description
1	IC(10)	19-20	12	option to print above in MKS units ON: IC(10) = 1
1	IC(11)	21-22	12	scale on Time Effect Plots Each dot will be spaced by 10 ** (IC(11))9 < IC(11) < 99 Default: .05, 1-5 hrs.
1	IC(12)	23-24	12	IC(12)=0 calculates design values and option for plots. IC(12)=1 no design values calculated and no plots printed IC(12)=2 no design values calculated, but option for plots.
1	IC(15)	29-30	12	debug printout for Stacy-Mihram method
1	IC(16)	31-32	12	number of double pages on plot Default: I double page minimum is I double page (2 pages)
1	IC(20)	39-40	12	<pre>IC(20)=1: Use maximum likeli- hood method in estimating parameters Otherwise: Use Stacy-Mihram method</pre>
1	ISTOPD	41-50	110	Number of increments in excess of 200 to be used in determining various statistical measures. Recommended value is zero or one.
1	IPLOT	51-55	15	<pre>IF IPLOT ≠ 0, Calcomp plots will be generated</pre>
1	IRAY	56-60	15	IF IRAY ≠ 0, Rayleigh distribution will be generated

Card	<u>Variable</u>	Cols.	Format	Description
1	CONVER	61-70	F10.0	Conversion factor to go from English to MKS units
1	CAL	71-80	F10.0	Conversion factor of input data to measurement desired
2	IOP(1)	1-2	12	<pre>IOP(1)=0: c = 2.0 as initial guess for use in Wegstein iteration IOP(1)=1: Initial c value read in.</pre>
2	IOP(2)	3-4	12	<pre>IOP(2)=1: Write initial c value</pre>
2	IOP(3)	5-6	12	IOP(3)=1: Write c, m, $\lambda$ estimates obtained by maximum likelihood estimation
2	IOP(5)	9-10	12	<pre>IOP(5)=1: Debug printout</pre>
3	N	1-5	15	Total number of samples
3	K	6-10	15	Number of divisions
3	ALP	11-20	F10.0	Value of 1 - F(x) corres- ponding to the desired extreme value
3	DEL	21-30	F10.0	Division size
3	CMNT(1-5)	31-80	5A10	Description of the set of data
4	NL	1-10	110	Number of L values to be considered. Up to five can be used (See Equation 2.15 in Reference 2.)
4	ELL(1-5)	11-60	5F10.0	up to five values of L
5	X(1), H(1)	1-80	8F10.0	K pairs of ordinate and experimental density values to be analyzed 4 pairs per card.

Multiple cases are processed by stacking the data sets with the last card as a blank to serve as a flag indicating the last case. However, the option cards (first two cards) are only read once. A run consisting of two sets of data is illustrated in Figure 3.

```
XXXXXXX.CM77000.T200.F4.
CHARGE.TTTT.NNNNNNNNN.CC.K.
ATTACH.BIMAR . BBBBBBBBBBBB TD= TTTT-
ATTACH. MSRDC.
ATTACH.IMSL.
LOSET(LIB=IMSL/NSROC)
BINAR.
               1
  1 1
                                           F22 H 30
  311
        15
           0.01
                         12.0
                                                        9996.
                                   2499.
                                             4998.
              311.
                        833.
                                                                               .0174
                       18.
                                             30.
                                                         .0212
                                                                    42.
              .0075
                                    .0147
   6.
                                                                   nn.
  54.
              -0102
                       £5.
                                    -0351
                                             78.
                                                         .0020
                                                                               .001A
                                    -0005
                                            126.
                                                         .0005
                                                                   170.
                                                                               .0
                      114.
              .0005
  102.
                                                          .000 3
  150-
                                    •0
                                            174.
              • 0
                                     " P22 3F 10
                            3.0
  262
        14
               0.01
             262.
•01527
                           54 E .
                                     1638.
                                               3275.
                                                           5559.
                                                                   10.5
                                                                              .04962
                        4.5
                                  .03917
                                              7.5
                                                         .05089
  1.5
                                                                              .0190A
                                  -03435
                                             13.5
                                                                   22.5
             .05598
                       16.5
                                                         .04071
  13.5
                                             31.5
                                   .00763
                                                         .00382
                                                                   34 . "
                                                                              .00127
  25.5
             .01272
                        28.5
  37.5
             .00127
                        40.5
                                   .00254
RLANK CARD
```

FIGURE 3. CARD IMAGES FOR A TYPICAL COMPUTER RUN

#### PRINTED OUTPUT

The printed output is dependent upon the options that are chosen. A general description of the printout follows. A sample run is shown in Appendix B.

The first page consists of the user options chosen. The options are only printed once for all the data sets. The initial guess for c, the value of c at each iteration used in finding c and the estimated parameters are next, if maximum likelihood method is chosen. If Stacy-Mihram method is chosen the iterations for finding m are given.

The second page identifies the data set being processed. The number of observations, number of bins,  $\alpha$ , and bin size are next printed followed by the bin widths, the histogram data. Next the logarithmic moments of the data follows;  $\overline{y}$ , s, and T. The last items in the header are the calculated generalized gamma parameters m, c,  $\lambda$  as computed by the maximum likelihood method or Stacy-Mihram method.

Eight columns follow: the values of the random variable, the value of the random variable in MKS units if CONVER is given and Option 6 of the IC options is chosen, the corresponding Rayleigh predicted frequencies, the corresponding measured densities, the corresponding Rayleigh predicted densities and the corresponding generalized gamma predicted densities.

The values of L, the density function, the cumulative distributions, and corresponding random variables are printed for each value of L. These occupy eight columns of output arranged as follows:

Column 1 - running index

Column 2 - value of the random variable.

Column 3 - f(x), (Equation 1 in Reference 1)

Column 4 - f(x), (Equation 11 in Reference 1)

Column 5 -  $f(x)^L$ 

Column 6 - G(x), (Equation 12 in Reference 1)

Column 7 - h(x), (Equation 14 in Reference 1)

Column 8 - H(x), (Equation 15 in Reference 1)

The following page gives the Rayleigh design values for all L values.

The fourth page gives the generalized gamma design values for one L value. These include  $x_M$ ,  $x_0$ ,  $x_S$ ,  $x_G$ ,  $x_{GA}$ ,  $x_D$ , and  $x_{DA}$ . To the right of these values,  $x_0$ ,  $x_G$ ,  $x_{GA}$ ,  $x_D$ , and  $x_{DA}$  as computed by a table look-up procedure are printed. This page is repeated for each L value.

After these pages there is a comparison of design values for all L values. The next pages consist of a printer plot which show the measured density, the density as predicted by the generalized gamma function, and the density predicted by the Rayleigh density function.

The following pages consist of a time effect printer plot which give L in hours vs.  $x_{\bar D}$  and  $x_{\bar G}$ . The CalComp plots generated replicate the printer plots.

#### PROGRAM DESCRIPTIONS

# Main Program

The main program serves as a driver for the entire digital program. In addition, many of the required computations are performed in the main program. A description of program flow follows.

All data required for the program is read from unit 5. A description of this data is presented earlier in connection with the input data.

After reading the data, the moments of the logarithms of the random variables are computed along with the Rayleigh parameter and maximum histogram value. The normalized third logarithmic moment, T, is tested against the value -0.5. If T > -0.5, the case is not processed. The parameters m, c, and  $\lambda$  are computed by a call to subprogram GETCML via the maximum likelihood or Stacy-Mihram methods.

Once values for m, c, and  $\lambda$  are determined, the various statistical measures are computed for up to five values of L. The density functions and cumulative distributions are printed for each L value considered, followed by the extreme, most probable, and significant values. The extreme, most probable, and significant values are obtained by the Wegstein iterative method (see Subroutine WEG).

After the above computations are performed, CalComp and printer plots are generated. These consist of comparisons of the measured density function with the generalized Gamma density function and with the Rayleigh density function.

Descriptions of major FORTRAN symbols are presented in Table 2.

TABLE 2
MAJOR FORTRAN SYMBOLS USED IN MAIN PROGRAM

FORTRAN Symbol	Math Symbol	Description
N K ALP	N K α	total number of samples number of divisions value of 1-F(x) corresponding to
DEL NL	Δx -	the desired extreme value bin size number of L values
ELL ISTOPD	L -	array of L values number of increments in excess of 200 to be used in determining extreme values
X	X	array of ordinate values
Н	f	experimental density values
S	S	<pre>value related to second logarithmic moment</pre>
YBAR	<del>y</del> T	first logarithmic moment
T	1	value related to third logarithmic moment
R	R	Rayleigh parameter
C M	C	parameter c
AMBDA	m λ	parameter m, real parameter lambda
XO	X	ordinate value
FOXO	f(x;λ,m,c)	predicted density function
BFOXO	F(x)	cumulative distribution function
BFOXL	F(x) <sup>L</sup>	cumulative distribution raised to the Lth power
GOFX	g(x)	density function corresponding to F(x)
HLO	h(x)	asymptotic density function
HHO	H(x)	asymptotic cumulative distribution
XSUBM*	Хμ .	most probable value
XSUBO*	×o	value at which $F(x) = 2/3$
XSUBS*	x <sub>s</sub>	significant value
XSUBG*	× <sub>g</sub>	most probable exteme value

<sup>\*</sup>These symbols are used as labels in the printed output generated by the program.  $\dot{}$ 

TABLE 2
MAJOR FORTRAN SYMBOLS USED IN MAIN PROGRAM (Cont.)

FORTRAN Symbol	Math Symbol	Description
XSUBGA*	×ga	most probable asymptotic value
XSUBD*	xD	design extreme value
XSUBDA*	×da	extreme asymptotic value

<sup>\*</sup> These symbols are used as labels in the printed output generated by the program.

## Subroutine GETCML

<u>Purpose</u>: To determine the parameters of a generalized gamma distribution from statistical measures of input data by either Stacy-Mihram method or maximum likelihood method.

Usage: CALL GETCML(AT,U,E,S,YBAR,GAMMA,OOC,T)
COMMON/PARAMS/,/PRNT/,/HIST/,/INPUT/,/OPT/,/IOUNIT/

# <u>Subroutines and Subprograms Called:</u>

MLHCML	Maximum likelihood estimation
WEG	Wegstein iteration
PSI	Digamma function
PSI1	Trigamma function
DIST	Evalutes measured and observed
	frequencies and densities
MGAMMA	Gamma function

<u>Description of Parameters</u>: See Table 3.

# Remarks:

(1) If  $X_D$  does not converge, a check value is sent to calling routine.

TABLE 3
MAJOR FORTRAN SYMBOLS

<u>Name</u>	Location	<u>Description</u>
AMBDA	/PARAMS/	$\boldsymbol{\lambda}$ parameter of output distribution
С	/PARAMS/	c parameter of output distribution
М	/PARAMS/	m parameter of output distribution
X(I)	/INPUT/	random variable values
ICK1	/OPT/	Check value. If ICK1=1, c root was not found via maximum likelihood method
IOP(I)	/OPT/	options
YBAR	argument	logarithmic mean of input data
S	argument	second log moment of input data
τ	argument	third log moment of data
CMNT(I)	/INPUT/	header label for GETCML output
FOBS, FTH	/PRNT/	computed values for observed and theoretical frequencies
DENO, DENT	/PRNT/	computed values for observed and theoretical densities
00C	argument	reciprocal of c
ICK	argument	check value. If $X_{\overline{D}}$ does not
		converge, ICK=1 is sent back to calling routine.
U	argument	trigamma function of final m value
Ε	argument	digamma function of final m value

TABLE 3
MAJOR FORTRAN SYMBOLS (Cont.)

Name	Location	<u>Description</u>
AT	argument	absolute value of the third log moment of data
H(I)	/HIST/	densities corresponding to random variable values.

# Subroutine MLHCML

<u>Purpose</u>: To estimate parameters  $\lambda$ , c, and m by the maximum likelihood method for the generalized gamma function.

Usage: CALL MLHCML

COMMON/PARAMS/,/HIST/,/INPUT/,/IOUNIT/,/PRNT/,/OPT/

# <u>Subroutines and Subprograms Called:</u>

WEG	Wegstein iteration
PSI	Digamma function
F	Function of parameter c
G	Function used by WEG to determine c

# Description of Parameters:

<u>Name</u>	Location	Description
AMBDA	/PARAMS/	$\boldsymbol{\lambda}$ parameter of output distribution
C	/PARAMS/	c parameter of output distribution
M	/PARAMS/	m parameter of output distribution
X(I)	/INPUT/	random variable values
0(1)	/HIST/	densities corresponding to random variable values
IOP(I)	/OPT/	options
ICK1	/OPT/	check value. If ICK1=1, c root was not found

# Remarks:

(1) c is restricted to values greater than zero.

- (2) If a root for F(c) is not found, a check value is sent to the calling routine.
- (3) An initial guess for c for use in WEG may be read in. Otherwise a default value of 2.0 is used.

## Subroutine DIST

<u>Purpose</u>: To calculate frequency and density distributions for Rayleigh and generalized gamma distributions.

<u>Usage</u>: CALL DIST (all parameters and arguments are passed in COMMON Blocks)

## <u>Subroutines and Subprograms called:</u>

MDGAM evaluates incomplete Gamma function

## Description of Variables:

<u>Variable</u>	Location	Description
X(I)	/INPUT/	random variables values
H(I)	/INPUT/	array of histogram ordinates for input data
К	/HIST/	number of bins in input histogram
N	/INPUT/	number of observations in input histogram
FTH(I), FOBS(I)	/PRNT/	computed values for the observed frequency distri-bution and theoretical frequency distributions
DENO(I), DENTR(I)	/PRNT/	computed values for the observed density distri-bution and theoretical frequency distributions

<u>Remarks</u>: The input histogram need not be evenly spaced in the abscissa x.

Method: Generalized gamma cumulative distribution is evaluated by MDGAM. The density function is obtained by numerically differentiating the obtained cumulative. The Rayleigh density distribution is obtained in a like manner.

## Subroutine WEG

<u>Purpose</u>: To determine root of x = f(x) by Wegstein iteration.

Usage: CALL WEG (I, X, J, N)

# Description of parameters:

- I input, iteration count. Initialization action is taken when I = 1.
- X input, estimate of root of x = f(x). On output, refined estimate of root.
- J number of significant digits of accurary desired in x for solution -- used only in initialization.
- N output completion flag

O convergence not obtained

1 convergence is within given accuracy

<u>Remarks</u>: The function whose root is to be found is computed externally. The calling sequence is as follows.

- (1) Initialize by issuing CALL WEG (1, XG, J, N) where XG is the initial guess for the root and J is the tolerance described above. N is irrelevant.
- (2) Set up a loop to calculate XN=F(X) using output X from WEG
- (3) The simplest calling sequence would then be

- 1 CONTINUÉ
- C MAXIMUM NUMBER OF ITERATIONS REACHED WITHOUT CONVERGENCE STOP
- 2 CONTINUE
- C ROOT FOUND WITHIN TOLERANCE

<u>Method</u>: The Wegstein method refines the root of the equation x = f(x) by calculating an improved estimate  $x_{I+1}$  which is the intersection point of the line y = x and the secant line of f(x) based on the previous two evaluations of f(x). This method requires only one function evaluation per iteration.

The equation for the intersection point is given by

$$X_{I+1} = \frac{F(X_{I}) * X_{I-1} - F(X_{I-1}) * X_{I}}{F(X_{I}) - F(X_{I-1}) - X_{I} * X_{I-1}}$$

Completion code N is set 1 when

$$|X_{x+1} - X_x| < |10^x * X_{x+1}|$$

i.e., when the change in X between iterations is less than one part in  $10^{\rm J}$ .

Function PSI1

<u>Purpose</u>: To evaluate the trigamma function,  $\Psi'(x)$ 

Usage: PSI1(x)

Description of Parameters:

PSI1(x) - value of the trigamma function at argument  $X_{\downarrow}(Output)$ 

X - argument of the function (Input)

## Remarks:

- (1) Argument x must be greater than zero.
- (2) The trigamma function is the second derivative of the natural logarithm of the gamma function.

Method: For arguments greater than 13 an asymptotic expansion,

$$\psi'(x) \simeq \frac{1}{x} + \frac{1}{2x^2} + \frac{1}{6x^3} - \frac{1}{30x^5} + \frac{1}{42x^7} - \frac{1}{30x^7}$$

is used. The truncation error associated with the above expansion is less than 1 x  $10^{-10}$  for x > 13. For arguments between 0 and 13, the recursion relation

$$\Psi'(x) = \Psi'(m+x) + \sum_{i=1}^{k} \frac{1}{(x+i-1)^2}$$

is used, where m is chosen as the smallest integer for which  $x + m \ge 13$ .  $\Psi'(m + x)$  is evaluated by the previous formula. The formulas are obtained from Reference 8.

## Function PSI2

<u>Purpose</u>: To evaluate the tetragamma function,  $\Psi$ "(x)

Usage: PSI2(x)

## Description of Parameters:

PSI2(x) - value of tetragamma function at argument X (Output).

X - argument of the function (Input).

## Remarks:

- (1) argument must be greater than zero.
- (2) the tetragamma function is the third derivative of the natural logarithm of the gamma function.

<u>Method</u>: For arguments greater than 13, the asymptotic expansion,

$$\Psi''(x) = \frac{1}{X^2} - \frac{1}{X^3} - \frac{1}{2x^4} - \frac{1}{6x^6} + \frac{1}{6x^6} - \frac{1}{10x^{10}} - \frac{1}{6x^{12}}$$

is used. The truncation error associated with the above expansion is less than 1 x  $10^{-10}$  for x > 13.

For arguments between zero and 13, the recursion relation

$$\Psi''(X) = \Psi''(\chi + m) - \sum_{i=1}^{k} \frac{2}{(\chi + i - i)^3}$$

is used, where m is the smallest integer which satisfies  $x + m \ge 13$ , and  $\Psi''(x + m)$  is evaluated by the previous formula. The above formulas are obtained from Reference 8.

## Function PSI

Purpose: To evaluate the digamma function,  $\Psi(x)$ .

Usage: PSI(x)

# **Description of Parameters:**

PSI(x) - value of digamma function at argument X (Output)

X - argument of function (Input)

# Remarks:

- (1) Argument X must be greater than zero.
- (2) The digamma function is the derivative of the natural logarithm of the gamma function.

<u>Method</u>: For arguments greater than 13 an asymptotic expansion is used:

$$\Psi(x) \sim \ln x - \frac{1}{2x} + \frac{1}{12x^2} + \frac{1}{120x^4} - \frac{1}{252x^6}$$

The truncation error associated with the above expansion is than 1 x  $10^{-10}$  for x > 13. For arguments less than 13, the recursion relation

$$\Psi(x) = \Psi(x+m) - \sum_{i=1}^{k} \frac{1}{x+i-1}$$

is used, where m is the smallest integer which satisfies  $x + m \ge 13$ , and  $\Psi(x + m)$  is evaluated by the previous formula. The above formulas are obtained from Reference 8.

#### Subroutine MGAMMA

Purpose: To evaluate Gamma function

Usage: CALL MGAMMA (X, GAMMA, IER)

**Description of Parameters:** 

X - input, argument of Gamma function

GAMMA - output value of Gamma function at X

IER - error code

Remarks: This is a library routine supplied by DTNSRDC.

User must attach library (IMSL).

Error code meaning is unknown.

#### Subroutine MDGAM

Purpose: To evaluate incomplete gamma function

Usage: Call MDGAM(T, X, PR, IE)

## Description of Parameters:

T input, limit of integral

X input, exponent in integral

PR output, value of incomplete gamma function

IE output, error code

## Remarks:

- (1) This is a library provided by DTNSRDC
- (2) User must attach IMSL library
- (3) Meaning of error code unknown
- (4) Function evaluated is given by,

$$P(x,T) = \frac{1}{\Gamma(x)} \int_{a}^{T} u^{x-1} e^{-u} du$$

#### Subroutine HISTO

<u>Purpose</u>: To set up labels and plot the experimentally measured density function.

Usage: Call HISTO

<u>Subprograms and function called</u>: SCALE, AXIS, SYMBOL, LINE <u>Remarks</u>: This program takes the measured density, which is passed in COMMON and uses these values to generate data for a CalComp plot.

#### Function G

<u>Purpose</u>: To be used by WEG in evaluating the c parameter by the maximum likelihood method.

Usage: G(c)

Subroutines and Subprograms Called: PSI

# Description of Parameters:

G(c) - value of function (Output)

argument of the function (Input)

Remarks: c must be greater than zero.

<u>Method</u>: To implement the Wegstein technique the equation f(x) = 0 must be put into the form x = g(x). The equation used is given by

$$C = \frac{\sum_{i=1}^{N} o_{i}}{\sum_{i=1}^{N} o_{i} \ln x_{i}} \left[ \ln c + \ln \left( \sum_{i=1}^{N} x_{i}^{c} o_{i} \right) + \ln \left[ \frac{\sum_{i=1}^{N} \ln x_{i}^{c}}{\sum_{i=1}^{N} x_{i}^{c} o_{i}} - \frac{\sum_{i=1}^{N} o_{i} \ln x_{i}^{c}}{\sum_{i=1}^{N} o_{i}} - \ln \left( \sum_{i=1}^{N} o_{i} \right) + \ln \left( \sum_{i=1}^{N} o_{i} \right) \right]$$

O<sub>i</sub> is the density

 $X_i$  is the value of random variable

## Function F

<u>Purpose</u>: To evaluate the function used to find the c parameter by the maximum likelihood method.

Usage: F(c)

Subroutines and Subprograms Called: PSI

# Description of Parameters:

F(c) - value of the function used to find the
 parameter c (Output)

c - argument of the function (Input)

Remarks: c must be greater than zero

Method: The equation used is given by

$$F(c) = \ln c + \ln \left( \sum_{i=1}^{\infty} x_i^* \circ_i \right)$$

$$+ \ln \left[ \frac{\sum_{i=1}^{\infty} \ln x_i (x_i^* \circ_i)}{\sum_{i=1}^{\infty} x_i^* \circ_i} - \frac{\sum_{i=1}^{\infty} \circ_i \ln x_i}{\sum_{i=1}^{\infty} \circ_i} - \ln \sum_{i=1}^{\infty} \circ_i \right]$$

$$+ \psi \left[ \frac{1}{c \left( \frac{\sum_{i=1}^{\infty} \ln x_i (x_i^* \circ_i)}{\sum_{i=1}^{\infty} x_i^* \circ_i} - \frac{\sum_{i=1}^{\infty} \circ_i \ln x_i}{\sum_{i=1}^{\infty} \circ_i} \right) \right]$$

$$- \sum_{i=1}^{\infty} \frac{1}{\sum_{i=1}^{\infty} \ln x_i} \left( \sum_{i=1}^{\infty} \sum_{i=1}^{\infty} \left( \sum_{i=1}^{\infty} \ln x_i \right) \right) = 0$$

$$= 0$$

O, is the density

 $X_4$  is the value of the random variable

## CONCLUSIONS

An extensive study of an existing digital computer program for determining parameters required to represent SES 100B trials data by a generalized gamma function was carried out. Difficulties encountered in earlier studies in which approximately 5 percent of the cases analyzed produced unrealistic values for the distribution parameters have been resolved. In order to resolve this problem, data sensitivity studies were carried out and three other techniques besides the Stacy-Mihram method were investigated. Based on results of the study, criteria are developed for determining cases that should not be processed. A summary of major conclusions follows.

- a. The Stacy-Mihram, maximum likelihood, grid search, and nonlinear least squares methods all yield estimated probability distribution functions which represent very well the experimentally measured histograms.
- b. Design extreme values are more sensitive to the experimental measurements than to the numerical procedure used in determining the estimation parameters.
- c. In some cases the predicted extreme design values are unrealistically large whereas the significant values are realistic. Based on an analysis of over 100 cases, it is concluded that cases having a nondimensional third logarithmic moment greater than -0.5 produce unrealistic extreme design values. Results of a data sensitivity

study have revealed that in all these cases the data may not be considered as a sample taken from a steady-state random phenomenon, and hence it is recommended that statistical analyses for these cases not be carried out.

- d. The Stacy-Mihram method should be used when the number of bins (number of divisions used in the analyses) is small (< 20) and when the number of samples is large (> 100).
- e. The maximum likelihood method should be used when the number of bins is large (> 60) or when the sample size is large (> 100).

## **ACKNOWLEDGEMENTS**

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# APPENDIX A COMPUTER PROGRAM LISTING

```
PROGRAM ORIGINAUT, CUTAUT, TARES-INAUT, TARES-OUTAUT, TARES-OUTAUT, TARES
        TEAL MAXX
        SEAL V
        OIMENSION XU(500).Z(500).FM(500).PM(500).IVAP(4)
        DIMERSION XAMS(500).FRMMS(500).FRMMS(500).FM(500).
DIMERSION XAMS(500).FRMMS(500).FR(00).BF0L(200).
       430FX4(301)+HL0MS(200)+H4945(100)
        ?IMEMSION PDX(7)+ELT(7)+FSC(7)+PQXM(7)+FGX(7)+RGXM(7)
        COMMON/I'PUT/X(160).FLL(7).N.ALP.O(160).ISTOPO.IPLOT.IPAY.IC.20)
        COMMON /OPT/IOP (20) . ICK1
        COMMON/PLO/NRUN + NPLC T+ ITP(4) + ITY(4) + ITY(4) +
       $""JMOA3,"AX$C$,$CA(10),FOOM(12)
        COMM ON ADAMT AFORS (100) .FTH (100) .DENT (100) .DELT (100)
      S.FTHP(196) + UFNTY (196) + CAL
COMMON PHISTS PHIRSTY + DELY
COMMON PHISTS PHIRSTY + DELY
COMMON PHIST PHIRSTY + CANT (S)
        COMMINIONARAME / MAMBOA . C.P
        COMMON ATOUNITAIDE. IRD. INST. IRCH
        DATA IDB . IPD . IWPT . IPCH/6.5.6.6/
        DATA XLENGYLENZIO.GA.Z
        TT4=2./T.
        CALL PL" 15(3.3.7)
        SHOTTON CARE
 PEAD (5.15) (TO(I).1=1.20) ISTOPH.IPLOT.IRAY.CONVER.CAL 4FITE(6.1413) IFLOT.IRAY
1413 FORMAT(141.754 IC OPTIONS USED IN THIS RUN SET TELOT=.IF.TY.
      $ 5 H I P AY = + 15 >
        00 14 T=1+20
    14 IF(IC(I).GT.0) WPITF(6.1414) I,IC(I)
 1414 FOR MATCHE . 3H OPTICE . 12.14=.121
WPITE(6.2013)
 2013 FORMAT (1H3.37HICP OPTIONS USED IN THIS PUN SET)
        READ(5.115) (ICP(I).I=1.20)
  115 FORMATIONIES
        00 979 I=1.20
        IF(IPP(I).6T.3) WRITE(6.1414) (1.10P(I))
  979 CONTINUE
        IF(COMVER-EQ.C.) COMVER=1.0
        FOR MAT (2012.110.215.2F10.0)
    99 CONTINUE
        45(1)=r.
        FMC10=0.
        7 P= 1
        25(1)=0.
        KLL = XLEY+2
                ***** READ INPUT AND PRINT ****
        READ (5-100) "-K-ALP-DEL-CYNT
IF(K-EG-0) 90 TO 10003
 170
       FOR MAT (215-2F10-0-5A10)
        PEAD L VALUES
        "EAD (5 -1 12) "L+(ELL(I) - I=1-"L)
        FOR MAT (112.7F16.0)
102
        READ(5+101)(X(I)+H(I)+I=1+K)
```

١,

```
131 FORMAT( PF10.0 )
230 FORMAT( 1X. 2315.4 )
        THA = 1.-ALP
¢
     IF UNEOUAL INTERVALS DELET
     DEL READ IN FROM X ARRAY

IF STARTING POINT N.E. 6.5 - SIGN WILL PRECEED

THE STARTING VALUE GIVEN AS DEL.
       DYX =DEL
       IF(DEL.67.0.0) 50 TO 199
       ST=+DEL
       0(1) = x(1)
       0 SU M = D (1)
       ¥ (1 ) =5 T
       DMX = D(1)
       JO 196 1=2.4
       ○(I)=x(I)
       IFCCCID.SE.D(I-1)) 2"X=0(T)
       X(I) = X(I-1) + C(I-1)
       SINUCIDED(I)
       DSU"=0SU"+8(1)
       CONTINUE
195
       TF(10(3) 4E0.0) TFL3≈1
       IF(IFL9.E9.1) GO TO 10007
       30 TO 137
  199 30 199 I=1.K
  198 0(1)=DEL
  197 CONTINUE
    OPTION 1: CONVERT INPUT TO DENSITY IF 'ECESSARY IF(IC(1).NE.1) 00 TO 0 00 II I=1.*
       \dashv(I) = \dashv(I) / (FLOAT(N)+^{\circ}(I))
11
     DETION 2: MODIFY L VALUES IF NECESSARY
       IF(IC(2).NE.1) 30 TO 3
       PTIME = ELL(1)
       00 12 I=1.NL
FLT(I) = FLL(I)
       ELL(I) =(ELL(I)/PTIME)+'
12
     OPTION 3: ADJUST IMPUT V(I) TO MICPOINT OF INTERVALS IF MECERSIAN
       IF(IC(3).NE.1) GC TO 4
3
       00 13 I= 1. K
     X(I) = X(I) + D(I)/2.5
OPTION 4: CONVERT INPUT TO MESSUREMENT DESIRED
       IF(IC(4).NE.1) 50 TO 5
       70 7 I = 1+K
H(I) = H(I) / C4L
       D(I)=D(I)+C4L
       X(I) = Y(I) + CAL
       CONTINUE
     IF L VALUES ARE DEAD IN AS SAMPLES DER TIME INTERVAL COMPUTE TIME VALUES FOR PLOT
С
       IF(IC(2).E0.1) 60 TO 6
       RTIME=FLL(1)/"
       00 57 I = 1.NL
       ELT(!) = FLL(!) + PT!YE/"
```

```
CONTINUE
5
       P=3 .
       YMAX =0 .
       SH=9.
       S1 = 0.
       S2 = 0.
       S3 = 3.
               ***** COMPUTE P. YI
       00 1 I=1+K
T1 =4(I)+0(I)
       IFCT1.TT.YMAX)YMAX=T1
       P=R+T1+X(T)++2
       ((I)Y)acla=IY
       SHESH+T1
       Y!3=Y[ •Y[
       Y13 = Y1 + Y 12
       $1=$1+T1 +YT
       $2=$2+T1 +YT2
       93=83+T1+Y13
     1 CONTINUE
              ***** COMPUTE YPAO. S. T *****
      ミジェル
       YRAP=S1
       T1=EN/ (EN-1.)
       T?=T1+EM/(EM-2.)
       73=S2
       T4= Y8A P+ Y8AP
       T5=T4+CH
       T= T2+(T3+2.+T4+TF)
T= T2+(S3+3.+YEAR+T3+YEAR+(3.+T4+T5))/S++1.5
IF(T.ST.(-.5)) WRITE(6.1237)
 1237 FORMAT(140.45HT IS SPEATER THAN -.5 GO ON TO NEXT DATA SET)
IF (T.GT.(-.5)) GO TO GR
       AT=ABS(T)
000
              **** COMPUTE M.C.LAMPDA. AND GAMMA *****
       CALL GETCML(AT-H-E-S-YB:P-GAMMA-000, T-ICK)
IF(ICK-EG-1) GO TO 59
       ICK = n
       IF(ICK1.FG.1) GC TO 59
       VRITE(F+R014)
9014 FOR MATEL HI-22HRAYLEIGH DESIGN VALUES )
       DO RE12 U=1+"L
XPD=SQRT(R+ALOG(FLL(U)/SLP))
       XRD MS=XRC+CONVER
       URITE(6+P013) ELL(J) +XRD+XRD4S
9112
       CONTINUE
      FORMATTIH +3FL= +F10 +4+ "X+RHXRSUED= +F10 +4+5Y+13HXRSUPT(YKS)= +
8013
      $F13.4)
       TFEICE121.F9.1) 90 70 19094
ç
               ***** COMPUTE C. Y. LAMPDA PRODUCTS FOR LATER UST
```

· ---

```
T1 = C+"
       T1M = T1-1.
T2 = (C+AMBDA++T1)/34MM4
       T9 = A89(T2)
       CM43C=T1"+00C
C
              ***** 10000 LOOP --- OVER THE L VALUES *****
       30 10000 IL=1.NL
                      ** INITIAL GUESSES FOR X AND X
       TXD = 1000.
       EXG = 0.
EXG = 0.
TYG = C.
       TX3 =1000 .
       5 x 0 = 0 .
       TYS4=9.
       5x34=6.
       TYDA=1 100.
       EYDA =0 .
EY0450.

EL = ELL(IL)

#PITE (6+10001) EL

19001 FOR MAT(1H1+3-L= +F7-1/)

IF (EL -5T- 300) GO TO 9001

EML = EYP(-EL)

30 TO 8002
 8001 EML = 5.
9002 CONTINUE
       IF(IC(9).E0.C) WRITE(6,304)
  ISTOP = 200+1ST2P9
                      ** SET UP HISTOGRAM PARAMETERS **
С
       I = 3
       J=0
       31VLn=y(1)-0(1)/2.
       MAX X=2 +0"X+XLEN
       YO= X(1)-0(1)
       Y00=X0+D(1)/2.
       IF(X0D .LE. .31) X0=0.
  701 IRES=1/2
       RES=(FLOAT(I)/2.)-IRES
       IF((PES-59-0),AMD.(J.LT.P)) J=J+1
       SELL = 0 (J) /2 . 0
       OFINC=D(U)/10.0
       X 0= X 0+ OF TNC
       I = I + 1
IF (I -97. TSTOP ) 90 TO 11002
YTO = YO
       ** 11030 L30P **
99 11096 IF=1*5
C
              ***** COMPUTE SMALL FOX) + PROPABILITY DENSITY FM *****
       YO = XT0+OFIAC+(IF-1)
```

```
T4=X3++T1*
        T45= (4 480A + 7 1) + + E
        75 = E40 (-T4F)
        FOX 0 = T3+T4+T5
C
        IF(IL.ST.1) 50 TO 19002
IF(XC.ST.MAXX) 50 TO 19002
IF(IP.E9.500) GC TO 19002
С
        IP=IP+1
        FM(IP)=FOXO
        MACIP) = MO
        Y T1 = X0 /R
        YT2=X0 +X T1
        PNX = 2 . + Y T1 + F Y P ( - X T2 )
        THE TES -PAY
        IFCRMX.GT.YMAX)YMAX=""X
        IF(FOXO.GT.YMAX)YMAX=F0 40
10002 CONTINUE
C
                ***** COMPUTE CAPITAL F(X). PROPABILITY DISTRIBUTION FM ...
        CALL MCGAMITAS .M.PR. IF)
 IF (IE.SC.129.CR.IE.EQ.130) WRITE (4.501) IE
531 FORMAT(59H FOROR IN GAMMA DISTRIBUTION EUNCTION COMPUTATION. EFPO
      .RE ,18)
IF (C .LT. g.) PR = 1.-PR
BECK( = PR
C
        TTT = FL+ALDG(RFOXD)
        TE (TTT-LT--300-) 30 TC 9003
        DFDXL = BF0x0**EL
90 T0 9004
 9003 PEDYL = 1.
 and4 CONTINUE
Ĉ
                **** COMPUTE SMALL G(X), SMALL H(X). CAPITAL H(X) *****
¢
        IF(IC(12).E0.2) 00 TO 11000
        GOFY = EL+(PFOYL/BFGXG)+FGXG
        EX = EL+(PR-1.)
        IF (EX.LT.-300.) GO TO 8010
        EX = EYP(EX)
        HLD = EL .FTYC+EY
        90 TO 8011
 8010 HL0 = 0.
       HHO =-E ML
 9011 CONTINUE
        IF (TF .GT. )) GO TO 11001

XOMS(I) = XO + CONVEP

FOXOMS(I) = FOXO / CONVER
        BFO(I) = BFOXO
        REPLIED = RECXL
GOEXMID = GOEY / CONVER
        HLOMS(I) = HLO/CONVER
        HHOMS(I) = HHO
```

```
1004 = I
      IF(IC(9).E0.1) 90 TO 11901
 WRITE (6.710) I.XO.FOXO.BECYO.BECKL.COFK.HLC.HHO
710 FORMAT(1X.IS.7915.6)
11001 CONTINUE
             ***** INITIALIZATION *****
С
      TX=APS(BFOXL-OMA)
      IF (*X-TXD) 9000+9001+9001
 9000 TXD = TX
      540 = 43
 2001 CONTINUE
      IF (TXG.GE.FOFX) GO TO 9002
      TX9=90FX
      EYS=YO
 9902 CENTINUE
      TX=ABS(PFOXA-TTH)
      IF (TX-TYO) 9003,9004,9004
 9003 TKG = TX
      EXD = XD
 3004 CONTINUE
      IF (TXSA .9E. HLS) 30 TO 9005
      TXS4 = MLC
      FYGA = X1
 9005 CONTINUE
      TX = ABS(HH0-044)
      IF (TX-TXDA) 9006,9007.2007
 9005 TXDA = TX
      EYDA = YO
 PUNTTHCD TODE
11003 CONTINUE
      YS=YTO+DELL
      IF (BF0x0.LE..999999) 50 TO 701
90 TO 11003
11002 WPITE (6.11004) ISTOP
11004 FORMAT (1x.+NO. 3F RECORDS ST+1X.TA)
11003 CONTINUE
      IF(IC(13).NE.1) GO TO 17
      WRITE(6,711)
FORMAT(//17,T40,13HM.*.S. SYSTEM//)
711
      WRITE(6,304)
      00 16 .= 1.1004
      #PITF(6,710) U, YOMS(U).FOXOMS(U).RFO(U).FFOL(U).SOFYM(U).
     (L)SMUHH (L)SMUHH
15
      CONTINUE
17
C
      CONTINUE
      IF(IC(12).Eq.2) 60 TO 970
000
             **** SOLVE FOR X
      T5=(M-000)++000
      XSUBY = T5/AYEDA
```

XSURMS = XSUPM + CONVER

```
WPITT(6.207) YSUBM.XSHPMS
      FORMAT(/2X+7HXSUEM= +F12+4+3X+12HXSUPM(MKC)= +F12+4)
              ***** SCLVE FOR Y USING WESSTEIN ITERATIVE METHOD
C
C
c
       T3=0MA++(1./EL)
       TT=ALP/EL
       \theta = \text{FXC}
      ME= 0
       CALL WEG (1.U.4.0)
C
                     ** START ITERATION LOCE **
    33 T45 = (AMBCA+U)++C
       CALL MOSAM(TAS.M.PR. 15)
       TF (C .LT. 0.) PP = 1.-PP
C
       11=U+TT+4L03(F9)
  CALL WEST2+U+0+NC)

ARITE (6+275) U+PR+TT+TT

205 FORMAT (1X++L= ++G20+R+FY++PP++G20+R+FY++T3++G20+R+5X++TT++F20+P)
      IF(U .LT. 2.) U=.0001
NE = ME + 1
       IF (ME .LT. 50) GO TO 7000
       WRITE (6.206)
 235 FORMATISAH TO CONVERGENCE ORTALTED FOR XCUPCI
       y = 0.
 3000 CONTINUE
       IF(NC.E2.G) 60 TO 33
                     ** END ITERATION FOR X
   32 X3UED = U
             **** EVALUATE GAMMA DISTRIBUTION FUNCTION *****
       TT= (AMEDA+U)++C
      CALL MORAME TT.M.PF.TE)
       JRITE 15.702) PR
  732 FORMAT (+ PR ++326.4)
             ***** SOLVE FOR Y USING WEGSTEIN ITERATIVE METHOD
C
      CA = C+A BDA
       09C4=1 .- C+4
      C43 = C+*-*.
      EL4 = EL-1.
      10 = EYS
      U = U0
VE = 0
 435 CALL WEGGI+U+4+0)
++ START TTERATION LOGS ++
       .J=0
   43 AU = AMPNA+U
      AUC = AU++C
TF(AUC -LT+ 20+) SO TO 4001
      U=1.E-10
```

```
30 TC 6982
 6001 CONTINUE
       EXPT = EXP(-4UC)
       FEELM+ (TO+EXPT+U++T14)++?
        CALL MOSAMIAUC.M.PR.IET
       IF (C .LT. 0.) PR = 1.-FR

U=F/((ER+U++CM3+5XPT+(OMSM+C+AUC))+T9)
 6002 CONTINUE
  CALL MER(2.00.0.9C)

WRITE (6.703) U.PR.F.CM3.EXPT.OMCM.AUC.AU.T2

703 FORMAT (* DEPUG *.5620.8)

IF (U.RE. 3.) RO TO 6003
        90=09+C(1)+2
        1 = 00
        90 TO 435
 SOUT CONTINUE
 THE = NE + 1

THE - NE + 1

THE (ME - LT - 50) SO TO 4000

WRITE (6+209)

ONE FORMAT (344 NO CONVERGENCE OBTAINED FOR XSUES)
        11 = 0
        30 T3 47
 4000 CONTINU
        IF("C.EG.G) 60 TO 43
C
                         ** END ITERATION FOR Y
    42 ¥$¥$6 = 0
 437 CONTINUE
С
                **** SOLVE FOR X USING WEGSTEIM ITERATIVE METHOD
C
000
        30 = X(K)
        VK=K/3
        10= Y(MK)
11= 10
15= 0
CALL WEG (1-0-4-0)
                          ** START ITERATION LOOP **
 5007 AU = AMPCA+U
        AUC = AU++C
        CALL MOGAMIALC . M.PR. IE)
        # (C .LT. 0.) PR = 1.-TR
        CALL WEG(2+11+0+11C)
#PITE(6+703) U+PP
IF (U+9E+0) GG TD 5004
C
        U=J3+D(1)
C
        " = U0
        3=1.E-13
  6004 CONTINUE
        ME = NE + 1
        IF (NE.LT.50) GO TO 6005
        WRITE (5.2090)
  2080 FORMAT (34H MO CONVERGENCE DETAINED FOR XSUBO)
        U = 0.
30 TO 4006
```

```
5005 CONTINUE
       IF(NC.F2.0) 50 TO 6307
                      TO TO 6007

** END ITERATION FOR Y
C
6006
      CONTINUE
       UMS = U + CONVER
       EXOMES = EXO + CONVER
       ARTTE(6.310) U.UMS.EYO.EXOMKS
       FORMAT(2x+*xSUB0= *+F12.4+3x+*xSUPO(*KS)= ++F12.4+3x+
312
      $ *TYSUED= *+F12.4+3X+*TYSUED(MMS)= *+F12.4)
              ***** COMPUTE SIGNIFICANT VALUE X
С
С
       IF (U .En. ).) U=EXA
       EMT=M+COC
       CALL MGAMMA (EMT.GAM. IER)
  IF(IE9.55.129.08.1E9.E0.140) WRITE(6.500)IF9
EDD FORMAT(464 E9ROR IN GAMMA FUNCTION COMPUTATION. EPRORE .19)
       AU = AMRTA+U
       AUC = AU ++ C
       CALL MESAM(ALC.EMT.PP.F)
IF (C .LT. 3.) PF = 1.-PR
       1=3 .+(1.-PR)+GAM/(GAMMA+4MPDA)
UMS = U + COMMER
       4717E(6.312) U.UMS
       FOR MAT (2 x + x SUBS= + + F12 .4 + 3 x + x SUPS( *KE) = + + F12 .4/)
312
       CONTINUE
5050
       YSUBAM = XSUBG + CONVER
       RRX(IL) = XSUBG
RGXM(IL) = YSUBGM
EXGM = ENG + CONVER
       ARITE(6.309) KSUBG. KSUBG. ENG. ENG.
       FORMAT(2X, 7HXSUBG= +F12.4.3X, 12HXSUPC(MKS) = +F12.4.3X.
      $ 8HTXSL89= +F12+4+3X+13PTXSUPG(MKS)= +F12+4)
                      SOLVE FOR ASYMPTOTIC VALUE OF Y USING VEGGTEIN METHOD
000
                       METHOD
       ELDG = EL/GAMMA

IF (C .LT. 9.) FLOG=-ELOG
       US = EXGA
       U = (UC+AMEDA)++C
       *1E = 0
       CALL 4E9 (1+U+4+0)
 ** START ITERATION LOGP **
5010 IF *U .LT. 309) GO TO 9501
       UT = 3.
       30 TO 8502
 8511 UT = U++"+EXP(+U)
 3502 13=C 4"0 C+FL CS+UT
       CALL WEG (2.U.D.NC)
       IF (U.6E.0.) GOTO 6011
       U0=U0+C(1)
       :J ≈ U0
       J=1 . E-10
 6011 CONTINUE
```

```
4F = 4E + 1
       IF (NE.LT.50) 30 TO 6012
       WRITE (4.2085)
 2395 FORMATICIFH NO CONVERGENCE CRIAINED FOR YOURGAD
      y = 0.
       WRITE(6.703) U.TOC.AMRDA.C
       50 TO 6913
 6312 CONTINUE
       TECHC.EG.US GO TO 6713

** END ITERATION FOR X
C
С
 6013 U=U++0CC/AMPCA
      UMS = L + CONVEP
EXGAM = EXGA + CONVER
       ARITECE+6014) U+UMS+FXG+FYGA
6314 FORMAT(2)x, *XSUBSA= *.F12.4.2)x, *XSUBGA(MKS)= *.F12.4.2)x.
E *FXSUFFA= *.F12.4.2)x, *TYSUBGA(MKS)= *.F12.4/)
6730 CONTINUE
      YSUBDM = XSUBD + CONVER POXYIL) = XSUBC
       SUSCA
      FXDM = EXD + CONVER
       4RITE(6+6015) XSHBO+XSUROM+EXD+EYOM
5015 FORMAT(2***XSUBD= **F12.4*2X**XSUPD(**S)= **F12.4*
     $ 3X . *TYSUBS= *.F12.4.3X . *TXSUBS(MKS) = *.F12.4)
              ***** SOLVE FOR ASYMPTOTIC VALUE OF X USING WEGSTET!
C
      UU =EL+ALOG(CMA)
      MO = EXDA
      U = U3
      "E = 0
       CALL WEG (1+U+4+0)
                     ** START ITERATION LOOP **
 5040 AU = AMBDA+U
       AUC = AU++C
      CALL MOGAM(AUC.M.PR.TE)
TF (C .LT. 0.) PP = 1...FP
U = U+LU
       ELPR = EL+PR
       UUU = SLPR
       IF(ELPP.LE.300.) UUU=ALOG(EYP(ELPR)-1.)
 8020 N = A-CAN
       CALL WEG (2.0.0.00)
       IF (U.CE.O.) 50 TO 6043
       UU=U0+0(1)
       U = U0
 6043 CONTINUE
       NE = NE+1
       IF(NE.LT.50) G7 TG 6044
       WPITE (5+2089)
 2089 FORMAT(35H NO COMVERGENCE DETAINED FOR XSUBDA)
      H = 0.
60 TO 6045
 5044 TECHC.59.07 TO TO 6040
                     ** END ITERATION FOR X
```

```
DA
                  UM = U + CONVER
                  ENDAM = EXDA + CONVER
6145 HRITF(6+6046) U+UM+EXCA+EXDAM
6046 FORMAT(2X9+XSUBCA= ++F12-4+2X+*XSUBCA(MKS)= ++F12-4+2X+

5 *TXSUBCA= ++F12-4+2X+*XSUBCA(MKS)= ++F12-4///)
10000 CONTINUE
                  ARITE(6.6047)
6047 FORMAT (1H1.T3.9HTIME (MIN).T20.9HTIME (HRS).T25.7HL VALUE.TE2.
               $5HX$UBE.167.5HX$UBG.T77.10HX$U80(MK$).T92.10HX$U8G(MK$))
                  00 98 I=1.%L
                  ESC(I) = ELT(I) / 60.0
                  ARITE(5.6048) ELT(I).ESC(I).ELL(I).ROX(I).PGX(I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((I).ROX((
                  CONTINUE
6048 FORMAT/14 +T2+F10+4+T19+F10+4+T32+F10+4+T47+F10+4+T62+F10+4+
$T77+F10+4+T92+F10+4)
С
     OPTION 5: PLOT HISTOGRAM WITH PLOTER PACKAGE 970 [F([C(5).LT.1] 30 TO 97
С
               COMPUTE HISTOGRAM VALUES
                  DIV=1.0
                  ICYT = 0
                   IF(IC(19).E9.1) DIV=D(1)
                   00 85 I=1+11
                  ICHT = ICHT + 1
Z(ICHT) = DEFO(T)/DIV
                   20 94 I = 2.8
                   If(IC(13).FG.1) DIV=D(I)
                   00 93 J = 1+10
ICNT = ICNT + 1
                   VIONCED = DENOCED/DIV
                  CONTINUE
94
                   PM = 9.0101
                   IPP = 20
                   K10 = 10+K
                   [PP = [Dr + 10
                   IFCRMCIPPI.LT.PM.AND.FM.(IPPI.LT.FM.AMO.ZCIPPI.FG.G.) 90 TO 83
                   IF(IPP.LT.KIS) SO TO 84
                   IP = IFP
                   IF(IP.LT.WIN) 60 TO 92
                  K11 = K10 + 1
30 90 I = K11+IP
 9)
                   2(1) = 7.0
9.3
                   CONTINUE
                   CALL INITPLA
             OPTION 15: NUMBER OF PAGES WEEDED FOR FLOT(DEFAULT=1 DOUBLE PG)
 С
                  MUMPAG = 1
                   TF(IC(15).NF.J) MUMPAG=IC(15)
                   MANSCA = ?
                   TVAR(1) = 1HY
                   IVARIED = SHYHIST
                   IVAR (3)=EHYGAYP
                   TVAR(4) = 4470AY
                   ITP(1) = 6HOHSERY
```

ITP(2) = 5HED .GA

.

```
ITP(3) = 64MMA AN
       ITP(4) = 640 RAYL
       ITP(5) = EHEIGH P
       179(6) = 6HEATS
       TTX (1) = AHVALUE
       ITX(2) = 640F PAN
       TTX (3) = 6HBCM VA
       ITX (4) = SHRIABLE
       ITX (5) = 64
       ITX (4) = 6H
       ITY(1) = 6HOENSIT
       ITY (2) = 6HY
       ITY(3) = 6H(AUP./
       [TY(4) = 6H8]N)/U
[TY(5) = 6H+8]U+4
       HTTIHE = (A)YTI
 TC(5) = 2 WRITE VALUES HEFORE PLOTTING

IF(IC(5) .EQ. 2) WRITE(6, 9190) (IVAP(I) .I=1.4)

9190 FORMAT(1HI.1) *.A1.10 *.45.6X.A5.6X.A4)
    XNMS(I) = YM(I) *CONVER

7*(I) = Z(I) / CONVER

FNMS(I) = FM(I) /COMVER

RNMS(I) = PM(I) /COMVER
       WRITE(3) (XUMS(T)+ZM(I)+FUMS(I)+FUMS(T))
81
       מי די די
       CONTINUE
A O
       00 91 I = 1. IP
IF(IC(5).50.2) WRITE(6. 9191) XN(I).Z(I).FN(I).RM(I)
 9191 FORMAT(14 +4F13-4)
       HAITECED CANCIDATOR *ENCIDARMOIDO
16
       CONTINUE
       CALL PLOTPR(3.4.IVAR)
97
       CONTINUE
    OPTION 7: TIME EFFECT PLOTS
       IF(IC(7).NE.1) 50 TO 95
C
    TEST TO SEE IN TIME EFFECT PLOTS ARE GOOD
       1FG1=0
       IF32=0
       TF(NL.E0.1) GO TO 95
       00 93939 II=2.NL
IF(IFG1.EQ.O.OF.IFG2.EQ.O) GO TO 95
С
       CALL INITOLO
    OPTION LES MUMBER OF PAGES MEDED FOR PLOTIDEFAULTED DOUBLE PGT
       YUMPAG = 1
```

```
IF(IC(16).NE.8) NUMPAG=IC(16)
      MPLOY= 2
      FROM(1) = 0.0
    OPTION 11: SCALE FOR IMDEFENDENT VARIABLE ON PLOTOFERAULT#.17
      SCA(1) = 0.05
      !F(IC(11).NF.0) SCA(!)=10**(IC(11))
      MAXSCA = 2
      ITP(1) = GHTIME E
      ITP(2) = SHFFECT
      ITP(3) = 6HPLOTS
      ITX(1) = 6HTIME I
      TTX (2) = 6HM HOUP
      ! TX ( 3 ) = 645
      ITY(1) = 640ESIR4
      ITY(2) = 6H VALUE
      ITY (3) = 5H
      ITY (4) = 5H
      IVAR(1) = 4HTIME
      IVAR(2) = EHYSUON
      IVAR(3) = GHXSURG
      IVAR (4) = 6H
    OPTION A: TIME EFFECT PLOTS IN MKS UNITS
С
      IFFICESTANEALD OF TO 60
      IVAR(2) = CHYD-MKS
      IVARIA) = EHXC+MKS
      ITY (3) = SH(4KS)
      00 61 0 = 1.9L
WRITE(3) (ESC(U).RDXM(U).R6XM(U))
51
      90 TO 65
63
      CONTINUE
      00 96 J = 1+NL
49[TE(2) (ESC(J)+RDX+J)+PGX(J))
95
      CONTINUE
65
      CALL PLOTPP (3.3. IVAR)
3 =
      CONTINUE
      IF(IPLOT.EG.O) GO TO 99
             ***** END 10000 LOOP
C
C
C
             ***** PLOT RESULTS *****
      CALL PLOTEYLL.B.+-3)
      CALL HISTO
      YN(IP+1)=FIRSTX
XN(IP+2)=DELX
      FN(IP+1)=FI7STY
      EN( 12+2) = DFLY
      RM([P+1)=FIPSTY
      PN(IP+2)=DELY
      CALL LIME(XN.FM.IP.1.0.1)
      IFFIRAY-EQ. 0) GO TO 10004
      CALL LIMECKNORNOTPOLOSOS
10004 CONTINUE
      60 TO 99
10093 IF(IPLCT-E9-0) STOP
      CALL PLOT(YLL.0..999)
      STOP
```

END

```
SUBROUTINE SETCML(AT.U.F.S.YBAR.SAMM1.00041....)
       COMMON /PAPAME/M. AMBPA.C.
       COMMEN AGETA I CR (20) + I CK1
       COMMON ATROUTAX (100) . ELL (7) .N.ALP .D(100) .ISTOPO.IPLOT.IPAY.IC(20) COMMON (PRNT/FORS(100).FTM(100).DENO(100).DENT(100)
      5.FTH9(100).DENT9(100).COMVER.CAL
       COMMONIMISTIFINED, K. BIM +(100). H(100). YMBY. YLEN, YLEN, CMNT (5)
       DIMENSION XMKS(100)+DELMKS(100)
       DIMENSION DHEAD(184)
       SEAL M
       1) DHS + CEILCR340 ATAC
       IF(IC(20).E0.1) 60 TO 5
              ***** SOLVE FOR " USING WEGSTEIN ITERATIVE METHOD *****
       "=5·
       "IE = 3
       CALL WEG (1.4,4+0)
C
              **** STERT ITERATION LOOP *****
     3 F=2511(M)
      U = PS 12 (Y)
       Y=M-AT-U/E++1.5
CALL WES (2.M.O.NC)
URITE(6.461) Y
  461 FORMAT (140.2HM=.E10.4)
       ME = ME+1
       IF(NE.LT.53) GC TO 2000
       #RITE(6+206)
  206 FORMATIZAH 10 CONVERGENCE CHTAINED FOR YSUPO)
       1 CK = 1
       BETHEN
 2000 IF(M.GE.C.) 50 TO 2001
       w = .0001
 2001 CONTINUE
       IF(MC.FR.S) BD TO 3
        ***** FND ITERATION FOR M
0000
              ***** COMPUTE C *****
      CONTINUE
       U1 = PSI(4)
       U2 = PSI1(")
       C = SQRT(U2/S)
       ! F ( T . G E . C . ) C = - C
       100 = 1./C
              **** COMPUTE LAMEDA *****
   4 AMBDA = EXP(-YBAR+U1+00C)
    5 CONTINUE
       ICK1=0
       IF(IC(20).E0.1) CALL MLHCML
       IFEICKI-ED-1) RETURN
       WRITE(6.191) CMNT
```

```
FOR MAT (1+1.5410)
       CMA = 1.-ALP
       ARITE (6.196) COMVER .CAL
       FOR MATCH #8+COMMER= #Fin.**#SX#20HCALIRRATION FACTOR= #F10.33
COMPUTE XCMKS) AND DELCMKS)
189
       30 17 LI=1.K
       DELMKS (JI) = D (JI) +CO'VER
       XMKS(JI) = X(JI) + CONVER
       FIND MKS VALUE OF YEAR
                              K+ALOG(CONVER)
       YBARMK = YBAR +
       WRITE(6.300) N.F.ALP.
                                            AMO
       FOR MAT ( / / 1 X + 3H1 = + 15 + 2X + 3HK = + 15 + 2X + 7HALPHA = + 91 1 + 4 + 2 X +
                                                         27.941-ALPHA= .310.4)
       #RITE(6+297)
  297 FOR MAT (/1X++DEL ARRAY+)
       JRITE(6.298) (DHEAD(I).T.D(I).T=1.K)
  298 FORMAT (1 + +4 (42+12+14)+F7+4+2X))
  IF(CONVER-NE-1) WRITE(6-296)
296 FORMAT(/1X++CEL ARRAY(MKS)+)
       TECCONVER-NE-1) WRITE(6-298) (OMEAD(I)-I-DELMKS(I)-I=1-K)
       WPITE(6.301) YEAP.YEARMY.S.T
      FOR MAT (/19.644848= +912.4+24.11H4840(MKS)= +812.4+2X+
      3 345= 4612.4.2X.3HT= 4612.4)
  203 FOR MAT (14, 3HM= .G12.4,34.8HLAMBDA= .012.4.34.3HC= .G12.4/)
              **** EVALUATE GAMMA FUNCTION
       IF(IEP.E1.129.09.IER.E0.130) WRITE(6.500)ICE
  500 FORMAT(1H +25HSTACY-MIRSAM PAR. AMECA=+F16-5+4H ME-F16-5+
     4 AH C=+F16.5)
       CALL DIST
       CMA =1 . -4 LP
       300=1./0
       CALL MEAMME (M.GAMMA. TER)
       AMK S = A MP CA / CONVEP
       PM(S = R + (CONVER**?)
                   STACY/Y
       MET=10F
       HOD = OH I HPAY
       IF(IC(20).EQ.1) MET=16HMAXIMUM LI
       IF(IC(20).EG.1) HOD=#HKFLIHOCO
       SPITE ( F. 302) M. C.AMBDA. AMKS. R. RMKS. MET. HOD
       FORMAT (/1X+3HM= +G12+4+2M+3HC= +G12+4+2M+8HLAMBDA= +
      1 312.4.2 V.1 TUL & MPDA (MKS) = .612.4.3HP= . 12.4.2HP (MKC) = .612.4.
      S/+7H . VIA +A10+A8+7H METHOD)
       WORD = 8 FR AYLE ISH
      WRITF(6:110) WORC-WOOD
FORMAT(TJ.PHVALUE OF.T19.8HVALUE OF.TT5.FHMFASURED.T51.

1AB .T66.5HGAMMA.T6.2.8HMFASUPEC.TSP.AB .T1
110
                                                                     .T114.5454444
     448
      $./.TA. CHRANDOM.T19.6HRANDOM.T35.9HFREQUENCY.T51.9HPREDICTED.T66.
      SOMPREDICTED. T82.7HDE"SITY.T98.9MPREDICTED.T114.9MPREDICTED./.
      ST3. RHV PRIABLE.TIP. BHVAR TAPLE.T51.9HFREQUENCY.T66.9HFREQUENCY.
      STR2.7H=/PIN/M.TR8.7HCENCITY.TI14.7HDENSTY././T20.5HCMKS))
WRITE(6.120) (Y(I), YMKS(I).FDRS(I).FTHP(I).FTH(I).DENO(I).
      SDENTR(I) .DENT(I) .I=1 .K)
      FOR MAT (T 3.F8.4.T19.F8.4.T32.F12.4.T49.F12.4.T63.F12.4.
      $T79 +F12 - 4 + T96 +E12 - 4 + T11 1 + E12 - 4)
       PETURN
       END
```

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```
SUBROUTINE HISTO
        COMMONIVHIST/BINLO+NOBING+BINW(100)+OPD(100)+YM4X+XLEU+YLEN+CMNT(5)
        CCMMON/HISTS/FIPSTX. DEL X.FIRSTY. PELY
        DIMENSION x(200)+Y(200)+RAY(5)
        12=10B TNS+1
         XAMY=(SV)CRC
           COMPLTE SCALE FOR Y-4YIS
            ORD IS THE ARRAY OF MEIGTHS FOR THE PINS
YER IS THE LENGTH IN INCHES OF THE Y-AXIS DEFINED IN

A DATA STATEMENT IN THE MAIN PROGRAM TO BE A INCHES
NO IS THE NUMBER OF POINTS IN ORD AND +1 SAYS EVERY POINT IS
                 TO BE PLOTTED
             FIRSTY THE FIRST Y VALUE ANNOTATED ON THE Y-AVIS IS RETURNED
            IN THE N2+1 LOCATION OF ORE
DELY THE SCALE VALUE - AMOUNT OF DATA PEP INCH- IS RETURNED
BY SCALE IN THE 12+2 LOCATION OF ORE
        CALL SCALE(OPD. YLEN. N2.+1)
        FIRSTY = ORD(N2+1)
        DELY=DFD(N2+2)
         TITLX=10HEXCURSIONS
        TITLY=745ENSITY
         ORD (12)=0.
             SCALES SET UP BY 4XIS TO BE USED BY LINE TO PLOT
            POINTS - X-AXIS LENGTH IS CONSTANT AND IS DEFINED IN A
DATA STATEMENT IN THE MAIN PROGRAM TO BE 10 INCHES
THE AXIS ANNOTATION WILL BE DONE WITHOUT THE USE OF
             THAT CO THAT THE NUMPERS LIVE UP WITH THE BINS DRAW!
        KOUNT = 1
        4 = 1
         0.C = (P)Y
         " = N+1
        IF (BINLC.ER.C.C) GO TO 5
         1 = N+1
        X(A) = BINTO
        12 = N2+1
       00 10 I=1.N2
         \chi(I) = \chi(I-I) + BI''A(\kappa GUNI)
        KOUNT = KOUNT+1
    10 CONTINUE
        CALL SCALE(X.XLE1.12.+1)
FIRSTX = X(12+1)
DELX = Y(N2+2)
        UNIT = 1./PELX
PUT PEW AT ORIGIN
С
        CALL PLOT(0 - +0 - +3)
        JO 20 I=1.M2
         STEP = Y(1) +UNIT
             DRAW AXIS PORTION FROM CUPRENT LOCATION TO END OF NEXT BIN
        CALL PLAT(STEP+0.+2)
             DRAW TICK MARK
        CALL PLOT(STEP .- . 1 . 2)
             AMNOTATE AXIS WITH NUMERALS
C
        CALL NUMBER (STEP==21:--21:-1:X(I):0.C:2)

RETURN PEN TO AXIS LINE WITHOUT DRAWING LINE
CONTINUE DRAWING AXIS AND ANNOTATING IT FOR THE PENALMPER
С
             OF THE VALUES
    20 CONTINUE
```

```
C
         TITLE THE AXIS
       CALL SYMPOL(4-25---32--14-TITLX-0-0-10)
       CALL AVISCO..O..TITLY.+7.YLEN.90..FIRSTY.DELY)
       RAY (1) =1 OH+RAYLE IGH
       RAY(2) = 10HDIST.
       RAY(3)=10H-COMPUTED
      RAY(4) = 10 HYALUE
RAY(5) = 10 H
      XPAGE=XLEM-2.8
      YPARE=YLEN-.5
      CALL SYMBOLIYPAGE, YPAGE .. 14, PAY(1).0.0.10)
      YPAGE=XP4GE+1.4
      CALL SYMBOL(XPAGE, YPAGE..14,RAY(2).0.0.10)
       XPAGE=XLEN-2.8
       YPAGE=YLEN-1.
       CALL SYMBOL (XPAGE, YPAGE, . 14.PAY(3).0.0.10)
       YPAGE=XP4GE+1.4
      CALL SYMBOL (XPAGE, YPAGE .. 14. PAY(4).0.0.11)
      XPAGE=XPAGF+1.4
       CALL SYMPOLITPAGE, YPAGE .. 14. PAY(5). C. 0 .10)
      YPAGE=XLEY-2.8
      YPAGE=YPAGE-.5
      CALL SYMPOL( MPAGE, YPAGE . . 14.CMNT . 3.0 .50)
      X (1) =B INLO
       Y(1)=0.
       X(2)=B INLO
       Y(2)=0RD(1)
      J=2
       00 1 I=1.409INS
      J=J+1
XT = X(J-1)+PINԿ(I)
      TX=(L)Y
      Y (J) =000 (I)
      J=J+1
      Y(J)=XT
      Y(J)=090(I+1)
      CONTINUE
      X(J+1)=F[RSTY
      Y(J+2)=0ELY
       Y(J+1) =F IRSTY
      Y (J+2)=0FLY
      CALL LINE(x, Y,J,1,0,0)
RETURN
      E 110
```

. ---

```
FUNCTION PSI1(M)
00000
                 FUNCTION PSI1 EVALUATES THE TRIGAMMA FUNCTION PSI (") FOR ARGUMENT N. PSII(M) IS THE DERIVATIVE WRT M OF THE
                 DIGAMMA FUNCTION.
          REAL W
          DATA C16.C130.C142/.166666667.033333333.0023839524/
С
          T1 = 0.
W = W
IF(#.5T.13.) 60 TO 2
C
         7 = 14. - W
W = 7 + D
O = 4 - 1
         0 = W - 1

00 1 I=1+N

T1 = T1 + 1./(0+I)**2

M-4T-13
c 1
         PCW = 1./W

RCW2 = RCW++2

PSI1 = RCW++(1.+PCW+(.5+PCW+(C16 +PCW2+(-C130 +PCW2+(C142 +PCW2+(C130)))) +TI
        PETURN
```

END

```
FUNCTION PSI2(M)

C

C

FUNCTION PSI2 EVALUATES THE TETPAGAMMA FUNCTION PSI (M)

FCR ARGUMENT M. PSI2(M) IS THE 2ND DERIVATIVE WRT M OF

THE DIGAMMA FUNCTION.

C

REAL M

CATA C16.C56/.166666667..8333333333/

C

T1 = 0.

M = M

IF(4.GT.13.) TO TO 2

M.LE.13

N = 14.-W

4 = M + N

D = M - 1

D0 1 I=1.N

T1 = T1 + 2./(D + I)**3

C

RCM=1./W

RCM2 = RCM+2

PSI2 = PCW2+(-1. +RCW+(-1. +RCW+(-.5. +RCW2+(C16. +RCW2+(-C16. +R
```

. ---

```
SUBROUTIME WESCI-XNP1-J-M)
                            00000
                                    INITIALIZATION
         IF(I.NE.1) 30 TO 2
      1 K = 1

xeV = xNP1

xTEMP = 10.**(-J)

xP = xVP1
         RETURN
                                    FIRST ITERATION
      IF(K.NE.1) GC TO 4

* IF(ARS(XP-XNP1)-YTE*P*ARS(XP)) 5.5.8

Q YP = X*P1
         X6NM1 = X8N
X8N = XMF1
         K = 2
      7 XN = XNP1
XMP1 = XPM
N = 0
         RETURN
      SUCCESTING ITERATIONS

4 XBNP1 = ((XMP1+YPNM1)-(YM+XBM))/(XMP1+XPNM1-YM-YPN)

IF((ABS(XP-YBMP1))-(12S(XTEMP+XP))) 5.5.6
      6 YP = XEVP1

XBNM1 = XBN

XBN = XEVP1

50 TO 7

5 V = 1
         PETURY
         END
```

SUBROUTINE AXIS
ENTRY LIME
ENTRY NUMBER
ENTRY PLOT
ENTRY SYMBOL
ENTRY PLOTS
RETURN
END

```
FUNCTION G(C)

COMMON/HIST/PINLO+K+PINW(100)+O(100)+YMAY+YLEN+YLEN+CMNT(S)

COMMON/HIST/PINLO+K+PINW(100)+O(100)+YMAY+YLEN+YLEN+CMNT(S)

COMMON/HIST/PINLO+CLE(7)+N+ALP+D(25)+ISTOPD+IPLOT+IRAY+IC(20)

CLNSUM=0+

SUMO=0+

SUMO=0+

SUMO+O(I)

CLNSUM=CUMO+O(I)

YLOSUM+ O/I)+ALOG(X(I))

YLOSUM= XLOSUM+ (X(I)+ALOG(X(I))

YLOSUM= XLOSUM+(X(I)+C)+O(I)

TOONTINLE

ARG= (XLOSUM/XOSUM)+(CLNSUM/SUMO)

S= (SUMO/OLNSUM)+ (ALOG(C)+ ALOG(XOSUM)+ALOG(ARG)+ALOG(SUMO)+

PSI(1-/(C+APO)))

PETURY

RND
```

```
SUBROUTINE MUHCHL
    MAXIMUM LIKELYHOOD ESTIMATION
      COMMON/HIST/GINLO.K.PINN(100).O(100).YMAY.YLEN.YLEN.CMNT(5)
      COMMON/INPUT/X(100).FLL(7).N.ALP.C(25).ISTOPP.TPLOT.IRAY.IC(23)
      COMMON ATTUNITAIDS. IRS. IRS. IPCH
      COMMON /P AR AMS/M. AMBO A.C.P
      COMMON/OPT/TOP(20) .ICK1
      REAL M
      IF(InP(1).NE.3)40 TO 10
  PAYLEIGH PAPAMETERS
      C=5 •
      อกไรก ฮอ
   13 READ (TR5 .131) C
  101 FORMAT(F10.0)
   30 TE(10P(2).E0.1) PRITE(1P6.102)
  102 FORMAT (140.20HIMITIAL GUESS FOR C=.F10.5)
      #PITE(IM6.555)
  555 FORMATELH +29MITERATIONS FOR FINDING C ROOT)
      WRITE( [P6.551)
  551 FORMAT(1" +8Y+14C+10Y+44F(C))
      KE=0
      00 1 I=1.51
      CALL WES(I+C+4+KE)
      IF(C.LT.C.) C=ARS(C)
      IF(C.ER.C.) C=-1
      491 TF ( 195+211) I+C+ZE90
 211 FORMAT(1H +12+F1C+5+F10+6)
IF(KE-E9+1)#C TO 22
      C=9(C)
    1 CONTINUE
C MAXIMUM NUMBER OF ITERATIONS REACHED WITHOUT CONVERGENCE
      TCX1=1
      WRITE (IP6.444)
  444 FORMATTINO.16HC POOT MOT FOUND)
      RETURN
   22 CONTINUE
   C ROOT FOUND WITHIN TOLERANCE
С
   FT"C 4
      xLOSUM=0.
      xosu~=e.
      DENSUM=0.
      SUMB =r.
      00 33 I=1.K
      YLOSUM=XLOSUM + ALOS(Y(T))+(Y(T)++C)+O(T)
      YOSUM=X0SUM + (X(I)++C)+0(I)
      OLNSUM=DLNSUM+ C(I)+ALCS(X(I))
      SUMO= C(I)+SUMC
   33 CONTINUE
      IF([])P(5).E3.1) WRITF([C9.111) XLOSUM.XCSUM.OLNSUM.SUMC
  111 FORMAT (1H) - 7-XLOSUM = -F10 -4-2 X-6H XOSUM = -F10-4-2 X-7HCL YSUM = -F10-4-
     $2X,5HSLM0=+F10.4)
      4=1./(C+((XL0SUM/XOSUM)-(OLNSUM/SUM0)))
C FOUND M--SOLVE FOR LAMBDA
      AM9DA=((XOSUM/(M+SUMO)) ++(-1./C))
      IF(10P(3).E0.1) WRITE(1PA.100)AMPDA.M.C.
  100 FORMAT (140,424PARAMETERS ESTIMATED BY MAXIMUM LIKELYHOOD.
     $11H EST[MAT[CN//1H .7HL4MANA=.F20.6.5x.2HM=.F10.6.5x.24C=.F10.6)
      PETURN
      FYO
```

```
TRIG BAITUOFBUR
                        REAL Y
                       COMMON/IMPUT/X(100) + ELL(7) + N + ALP + D(120) + ISTOP3+IPLOT+IRAY+IC(20)
COMMON/PARAMS/M+MBDA+C+R
COMMON/PARAMS/M+MBDA+C+R
COMMON/PARAMS/M+C(100) + FTH(100) + DENO(100) + DENT(100) + FTHP(130)
                     T.DENTR (100).CONVER.CAL
                         COMMONIMISTICINUO.K.RIMW(100).H(100).YMAX.XLEN.YLEN.CMNT/5)
                         90TTOM = 0.0
                        PMIN1 = 1.0
                        01V=1.0
                         0.1=20
                         00 10 I =1.K
            OPTION 18: IF ON DENSITY = (NO PRINTY NEW TENTE OF OF STREET NO PRINTY (NO PRINTY (NO PRINTY NEW TENTE OF TENTE
                        IF(IC(18).E7.0) CIV=D(I)
IF(IC(18).E7.1) D2=D(I)
                         ARGR=(Y(I)+9(I)/2.)++2./9
                        RI = EXP(-ARTR)
                        A93=(AMBOA+(X(I)+0(I)/2.))++C
                        CALL MEGAM (ARG. M.TOP. IEP)
C
                DRISER VED FREQUENCY
С
                       F03S(I)=P(I)+H(I)+N
                ORSERVED DENSITY
                        DENO(1)=4(1)+0?
C
                THEORETICAL PAYLEIGH (EXPONENTIAL) FREQUENCY
С
                FTHR(I) = (RMIN1 - R1 ) + M
RAYLEIGH(EXPOMENTIAL) DENSITY
C
                        DENTR(I) =(RMIN1 - P1)/DIV
С
                THEORETICAL GAMMA FREQUENCY
С
                        IF(IER.NE.0) 80 TO 10
                        FT4(I) = (TOP - BOTTOM) + N
                GARMA PREDICTED DESSITY
C
                        VICTOR- POTTOWN/PIX
                        PMIN1 = R1
                        SOTTOM = TOP
                        CONTINUE
10
                        RETURN
                        END
```

APPENDIX B
SAMPLE OUTPUT

I PA Y= 1C OPTIONS USED IN THIS RUN SET IPLOTE
2PTION 5= 1
0PTION 9= 1
0PTION 20= 1 INITIAL GUESS FOR C = 2,00000 ITERATIONS FOR FINDING C ROOT 1 2,00000 -.004530 2 1,93815 -.00446 3 1,89815 -.000400 4 1,88827 -.00002 5 1,88712 -.000000 10P OPTIONS USFD IN THIS RUN SET OPTION 3= 1

PARAMETERS ESTIMATED BY MAXIMUM LIKELYHOOD ESTIMATION

LAMBUA=

.978837 # .064866

C= 1.887116

P22 3F 10 CONVER= 1.000 CALIBRATION FACTOR= 0.000

N= 262 K= 14 ALPHA= .1010F-01 1-ALPHA= .9900

0000		238.7	2
5 (8) 3		R(MKS)=	101717171
17) 3.0000		238.7	MCACHDEN
14) 3.0000 D	0 a.	.6487F-01P=	110434
3.0000 B	1= -1.0	A (MKS)=	AMMA
DEL ARRAY De 1) 3.80000 De 2) 3.0000 De 3) 3.0000 De 4) 3.0000 De 5) 3.0000 De 6) 3.0000 De 7) 3.0000 De 8) 3.0000 (9) 3.0000 Deito) 3.0000 Deit) 3.0000 Deit) 3.0000 Deit) 3.0000 Deit4) 3.0000	S= .4751 T= -1.040	LAMBDA: .6487E-01 LAMBDA(MKS): .6487E-01R: 238.7 R(MKS):	DAVI CTCU
3.0000 D(	2.411	LAMBDA=	AU MEACHDED
3.0000 0(3)	YBAR(FKS)= 2.411	C= 1.9788 C= 1.987	ANTERNOOM NET HOU
DEL ARRAY Di 1> 3.0000 Di 2> 3.000 ' ( 9> 3.0000 Diio> 3.0000	YFAR= 2.411	.9788	VALUE OF SALES
DEL ARRAY D( 1) 3.00 . ( 9) 3.00	YF: AR =	===	4147

. VIA MAXIMUM	VIA MAXIMUM LIKELIHOOD METHOD	i					•
VALUE OF	VALUE OF	MEASURED	RAYLFIGH	CAMMA	HFASURED	RAYLFIGH	CAMMA
RANDOM	RANDOM	FREGUENCY	PREDICTED	PPENICTED	nENSITY	PREDICTED	PREDICTED
VARIABLE	VAR IARLF		FREQUENCY	FREGUENCY	=/BIN/N	DENSITY	DENSTIV
	(MKS)						
1.5000	1.5000	.1200F+02	.9696F+01	.1257E+02	.1527F-01	.1234E-01	.15996-01
4.5000	4.5000	.3000E+02	.2699E+02	. 10035+02	.3817E-01	.34335-01	. 3821 E-01
7.5060	7.5900	.4000E+02	.3872E+02	.39615 +02	.50895-01	.4926E-01	.5040E-01
10.5000	10.5000	.3900E+02	.4 124F +02	.4204F+02	.4962E-01	.55085-01	.53485-01
13.5000	13.5000	.4400F+02	.4124E+02	. 1884E+02	.559RE-01	.5247E-01	.49425-01
16.5000	16.5000	.2700E+02	*3465E+n2	.3224E+02	.34355-01	.4409E-01	.41025-01
19.5000	19.5000	.32005.+02	.2612E+02	.2443F+02	.4071F-01	.332 3E-01	.3108F-01
22.5000	22.5000	.1500E+02	.1784E+02	.170 6E +02	.1908E-01	.2269E-01	.21705-01
25.5000	25.5000	.9998E+11	+1110E+02	.1104F+02	. 1272E-01	.1412E-01	.1405E-01
28.5000	28.5000	.5997E+01	.6319E+01	.66555+01	.7630F-02	.8039F-02	.8467E-02
31.5000	31.5000	.3003[+0]	.3301E+01	.3746F+01	.3820F-02	.4199E-02	.4766E-02
34.5000	34.5000	.99825+00	.1585F+01	.1974E+01	.1270E-02	.2017E-02	.2511E-02
37.5000	37.5000	.99R2E+00	.7009E+00	.9754E+00	. 1270f -02	.891RE-03	.12416-02
40.5000	40.5000	•1996E+01	.2857E+00	.452RE+00	.2540E-02	.36355-03	.5761E-03

49.2759 51.0232 53.5310 XR SUPDEPKS) = XR SUPDEPKS) = XR SUPDEPKS) = 49.2759 51.0232 53.5210 RAYLFIGH DESIGN VALUES

L= 262.0000 XRSUHD=

L= 546.0000 XRSUBO=

L= 1638.0000 XRSUBO=

XSUBH= XSUH9= XSUBS=	10.0849 15.2986 22.1135	KSUBM (FX S) = KSUBO (PK S) = KSUBS (MK S) =	10.0349 15.9986 22.1135	IXSUB0=	15.9000	TXSURO(MKS)=	15.9000
K SUBG=	38.4161	XSURG (MKS) =	18.4161	TXSURG=	38.4000	TXSURG(MKS)=	38,4000
XSUB GA=	38.4206	XSURGA (MKS) =	38.4206	TXSUBGA=	38.4000	TXSURGA(MKS)=	38,4000
KSUBD=	52.5000	XSUBD (MKS) =	52.5000	TXSUBD=	52,5900	TXSUBO(MKS)=	52.5888
XSUBDA=		XSUBDA (MKS) =	52.5001	TXSUBDA=	52,5000	TXSURDA(MKS)=	52.5888

I = SAG.

41.1000	54.6000 54.6000
TXSURGCMKS)= TXSUBGA(MKS)=	TXSUBD(MKS)= TXSUBDA(MKS)=
41.1000	54.6000
TXSUBG= TXSUBGA=	TXSUBD= TXSUBDA=
40.9344	54.6000 54.5996
XSUBG (HKS) = XSUBG A (HKS) =	KSUBO (PKS) = XSUBDA (PKS) =
40.9344	54.6000
XSUBG= XSUBGA=	X SURDE X SURDA =
	40.9344 XSUBG(HKS)= 40.9344 TXSUBG= 41.1000 TXSUBG(MKS)= 40.9670 TXSUBGA(MKS)= 40.9670 TXSUBGA= 41.1000 TXSUBGA(MKS)=

1638.0

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X SUBM= X SUB 0 = X SUBS=	10.0849 15.9986 22.1135	XSUBO (MKS) = XSUBO (MKS) = XSUHS (PKS) =	10.0849 15.9986 22.1135	TXSUB0=	15.9000	TXSUBO(MKS)=	15.9000
XSUBG= XSUBGA=	44.5527	XSUBG (MKS) = XSUBGA (MKS) =	44.5527	TXSUBG= TXSUBGA=	44.7000	TXSUPF(MKS)= TXSUBGA (MKS)=	44.700
X SUBD= X SUBDA=	57,3000	XSUBD (NKS) = XSUBDA (MKS)=	57.3000	TXSURD= TXSURDA=	57.3000	TXSUBDCMKS)= TXSUHDA(MKS)=	57,3000

X SUA GEMKS)	38.4151	40.9344	44.5527
KS HBD ( MKS)	52.5000	54.4000	57.3000
ASUPA	38.416.1	84 x 6 . 0 4	44.55.27
XSURD	52, 5000	54.6000	57.3000
L VALUE	272.0000	546.0000	16 38 0000
TIMF CHRS)	.0167	-0347	.1042
TIME CHIN)	1.0000	2.0840	6.2519

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A=VHINT B=Yth=M 0.0000 C=Yth=M 0.0000 M 0.0000 C=Yth=M 0.0000	9900°0	1020.		0040-		.0400		3000		1000
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INITIAL GUESS FOR C= 2.00000 ITERATIONS FOR FINDING C ROOT

2.00000 1.90360 1.90360 1.32413 1.22413 1.25413 1.25113 PARAMETERS ESTIMATED BY MAXIMUM LIKELYHOOD ESTIMATION

C

LAMBDA=

4= 1.758994 .038933

C= 1.251726

CONVER= 1.000 CALIBRATION FACTOR= 0.000

	PC 8312.0000	
	.0000 Of 3)12.0000 Of 4)12.0000 Of 5)12.0000 Of 6)12.0000 Of 7)12.0000 Of 8)12.0000	
	Df 6312.0600 Pf14312.0000	. P.245
•	D(5)12.0000 )(13)12.0000	T= P.245
HA= .990(	)12.0000 12.0000	S= .4901
1-ALP	0 0(4	
ALPHA= .1000E-01 1-ALPHA= .9900	11 112.000	BARCHKS)= 3.450
ALPHA = .	12.0000 D	YBAR ( MKS )
15	DE 1312.0000 DE 2312.	50
N= 311 K=	RRAY 12.0000 2.0000	YBAR= 3.450
"	OFL A D( 1)	YBAR =

DCT-C - WYOL	- COMPLETE OF		1064.	CF/2.0-1			
N= 1.759	C= 1.252	LAMPDA=	.3883F-01 LAMBDACKKS)=		•38A3F-01R= 2059.	R (MKS)=	2059.
. VIA HAXIMUM	LIKELIHOOD METHOD						ı
VALUF OF	VALUE OF	PEASURED	PAYLF16H	TAMA	MFASURED	RAYLFIGH	SAMMA
RANDOM	RANDOM	FREQUENCY	PREDICTED	PREDICTED	PENSITY	PREDICTED	PREDICTED
VAR TABLE	VARIABLE		FREQUENCY	FREGUENCY	= /BIN/N	DENSITY	DENSI IV
	(HKS)						
9	6.0000	.2799E+02	*2101F +02	.2809E+02	.7500F-02	.5630E-02	.7527F-02
18.0000	18.0000	.5486E+02	.5489E+02	. K607F +02	.1470E-01	.14715-01	.17705-91
30.000	30.000	.7912E+02	.693RE+02	. F981F +02	.2120E-01	18595-01	-18715-01
42.0000	42.0000	.6494E+02	.6416F +02	.5593E+02	.17405-01	.1719F-01	.14995-01
54.0000	54.0000	.3807F+02	.4744F+02	. 3847F+92	.10205-01	.1271E-01	-10315-01
9000-99	0000.99	.1903E+02	.2905F+02	.2390f +02	.5100F-02	. 778 3E-02	.64055-02
78.0000	78.0000	.141RE+02	.1497E+02	.1378F +02	. 3800F-02	.4012E-02	. 3691F-02
90.000	90.000	.59716+01	.4563E+01	. 748 3E +01	.1600E-02	.175AE-02	-2005E-02
102 - 0000	102.0000	.1866E+01	.2460F+01	.38715+01	.5000F-03	.6592E-03	.1037E-02
114.0000	114.0000	.1866E+01	.7920E+00	.19215+01	.50001-03	.2122E-03	.514RE-03
126.0000	126.0000	•1866E+01	.2195E+00	.9197E+00	.5000E-03	.5882E-04	.24645-03
138.0000	139.0000	•	.52516-01	.4264E+00	•0	.1407E-04	.11425-03
150.0009	150.0000	.0	.10855-01	.1921E+00	.•0	.290AE-05	.5146E-04
162.0000	162.0000	0.	-1940F-02	. R428F-01	•	.5199E-06	.2258E-04
174.0000	174.0000	.1120F+01	.30046-03	.3611F-01	. 30 0 0E - 03	.8050E-07	.9675E-05

145.9384 152.7299 159.9632 XR SUBDE WKS) = XR SUPDE WKS) = XR SUPD (MKS) = 145.9384 152.7299 159.9632 RAYLEIGH DESIGN VALUES
L= 311.0000 KRSUBD=
L= 833.0000 KRSUBD=
L= 2499.0000 KRSUBD=

44.4000	128.4000 128.4000	192,0000
TXSUBD(MKS)=	TXSURG(MKS)= TXSURGA(MKS)=	TXSURD(MMS)= TXSUBDA(MKS)=
0004***	128.4000 128.4000	192.0000
TXSUB0=	TXSUBG= TXSUBGA=	TXSUBD= TXSUBDA=
24.9272 44.9450 65.4169	128,546P 128,5892	192,0000
XSUBO (MKS) = XSUBO (MKS) = XSUBS (PKS) =	XSUBS (MKS) = XSUBGA (MKS) =	XSUBD (MKS) = XSUBDA (MKS)=
24.7272 44.9450 65.4169	128.5468	192.0003
X SUBM= X SUHO= X SU 6S=	xSUB6= xSUB6A=	X SURD= X SURPA=

L= 833.0

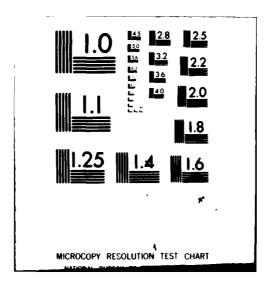
KSUBN= KSUBN= KSUBS=	24.9272 44.1450 65.4169	XSUBN (MKS) = XSUBN (MKS) = XSUBN (MKS) =	24.9272 44.9450 65.4169	TXSUB0=	000000	TXSUBD(MKS)=	0000
(SUBG=	143.0865 143.0789	XSURGENKS)= XSURGA (MKS)=	143.0865	TXSUBG= TXSUBGA=	142.8000 142.8000	TXSU46(MKS)= TXSUBGA(MKS)=	142.8000 142.8000
rsugn= rsugna=	205.2000	XSUBD (MKS) = XSUBDA (MKS)=	205-2080 205-2000	TXSUBD= TXSUBDA=	205.2000	TXSURD(MKS)= TXSURDA(MKS)=	205.2000

L= 2499.0

XSUBM= XSUB0= XSUPS=	24.9272 44.9450 65.4169	XSUBO (MKS) = XSUBO (MKS) = XSURS (MKS) =	24.9272 44.9450 65.4169	TXSUB0=	44.4000	TXSURO(HKS)=	0004*44
XSUBG= XSUBGA=	158.6699 158.6588	X SUBS (MK S) = XSUBGA (MKS) =	158.66 <sup>99</sup> 158.6588	TX SUBG= TX SUBGA=	158.4000 158.4000	TXSUBG (MKS) = TXSUBGA (MKS) =	158,4000 158,4000
XSUBD= XSUBDA=	219.6000	XSURD (MKS) = XSURDA (MKS)=	219.6000	TXSUBD= TXSUBDA=	219.6000	TXSUPO(MKS)= TXSUPOA(MKS)=	219,6000

TIME CHIM)	TIME (HRS)	LVALUE	GRUSX	98HS x	X SUBD (MKS)	X SUBG CMK S >
0000	19167	311.0000	1 72 - 0000	124.5468	192.0000	128.5468
2.6785	9440	9 3 000 0	205,2000	193.0865	205,2000	143.0865
40.0	1139	24.99.0000	219.6000	158.6699	219.6000	154.6699

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